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(54) **OPTICAL IMAGE CAPTURING LENSES**

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This patent is subject to a terminal dis-
claimer.

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Feb. 24, 2012, now Pat. No. 8,780,464.

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G02B 9/62 (2006.01)
G02B 13/00 (2006.01)

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CPC **G02B 9/62** (2013.01); **G02B 13/0045**
(2013.01)

(58) **Field of Classification Search**

USPC 359/713, 762, 761
See application file for complete search history.

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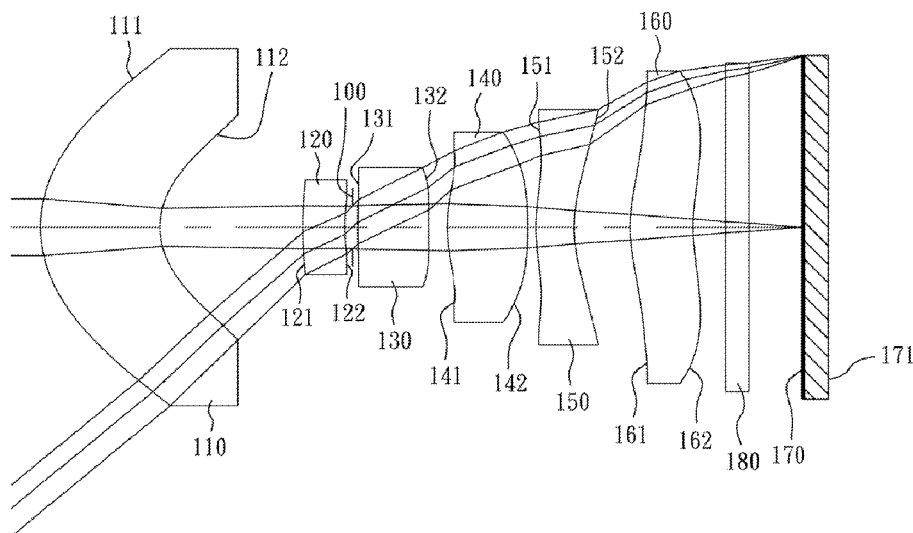
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(57) **ABSTRACT**

An optical image capturing lenses includes, in order from an object side to an image side, a first lens element with refractive power, a second lens element with negative refractive power, a third lens element with refractive power, a fourth lens element with positive refractive power, a fifth lens element with refractive power and a sixth lens element with refractive power. The first lens element has a convex object-side surface and a concave image-side surface. The second lens element has a convex object-side surface and a concave image-side surface. The fifth lens element is made of plastic material, and two surfaces of the fifth lens element are aspheric. The sixth lens element has a convex object-side surface and a concave image-side surface and is made of plastic material, the surfaces of the sixth lens element are aspheric, and the image-side surface thereof has at least one inflection point.

32 Claims, 15 Drawing Sheets



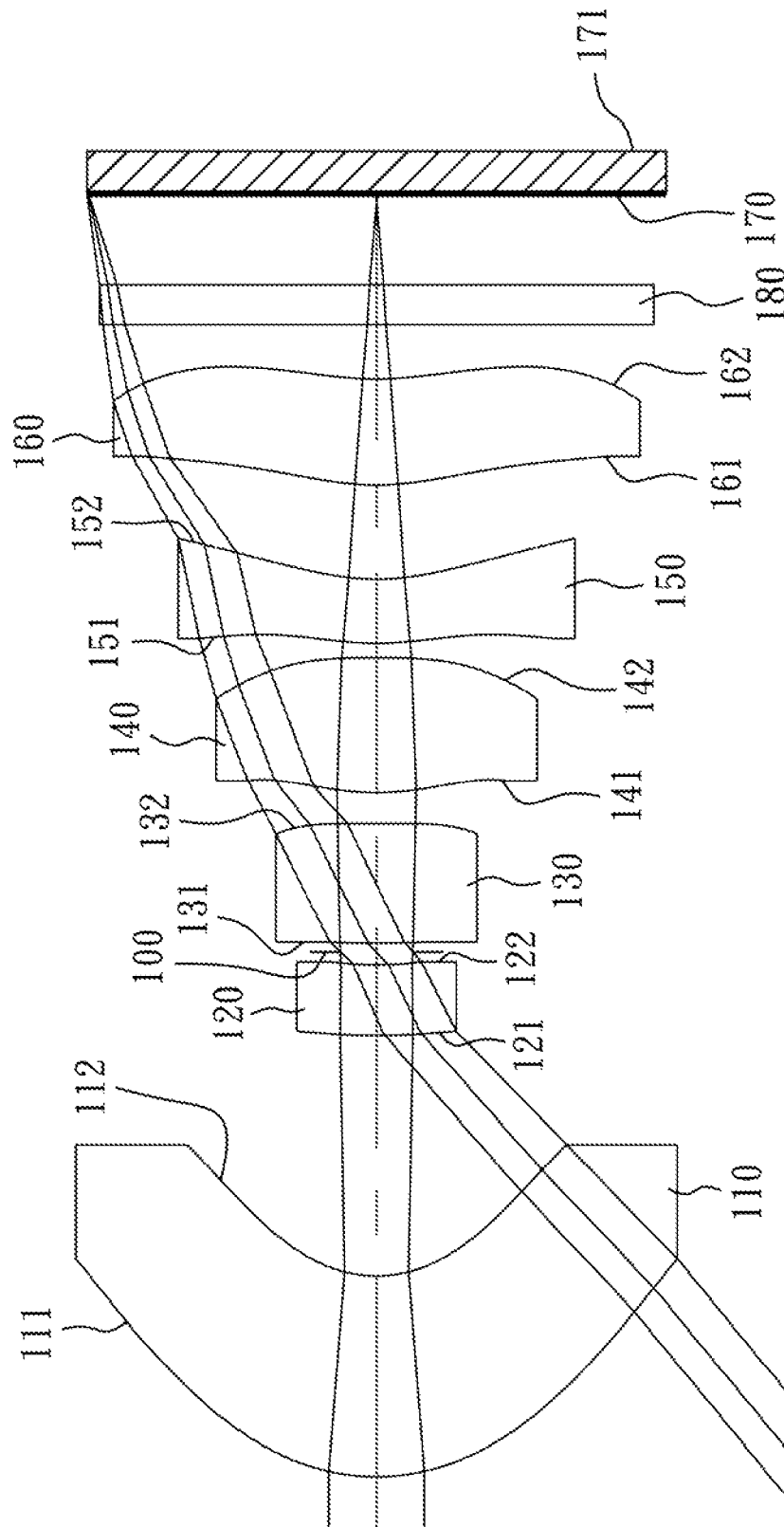


Fig. 1

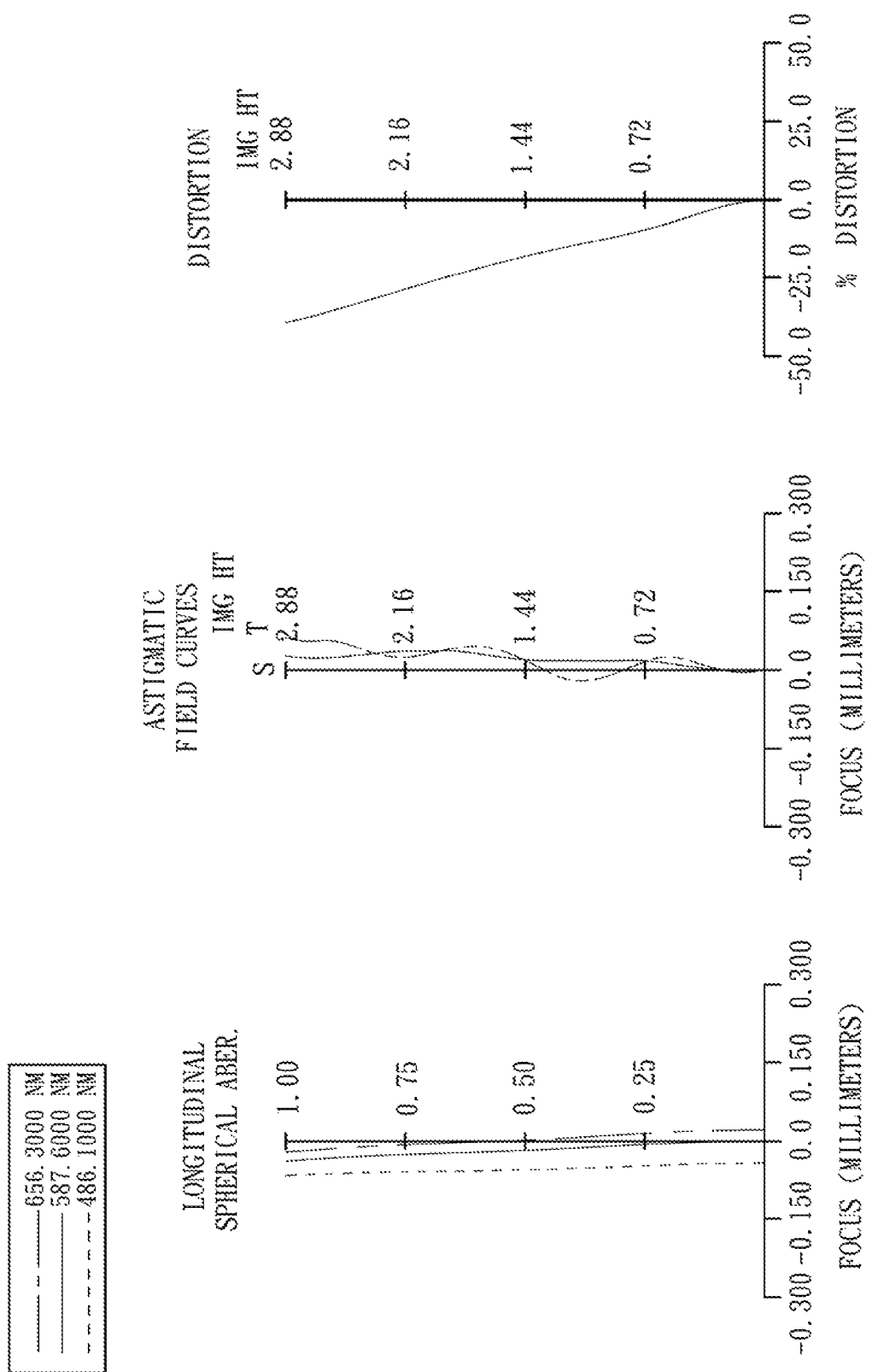


Fig. 2

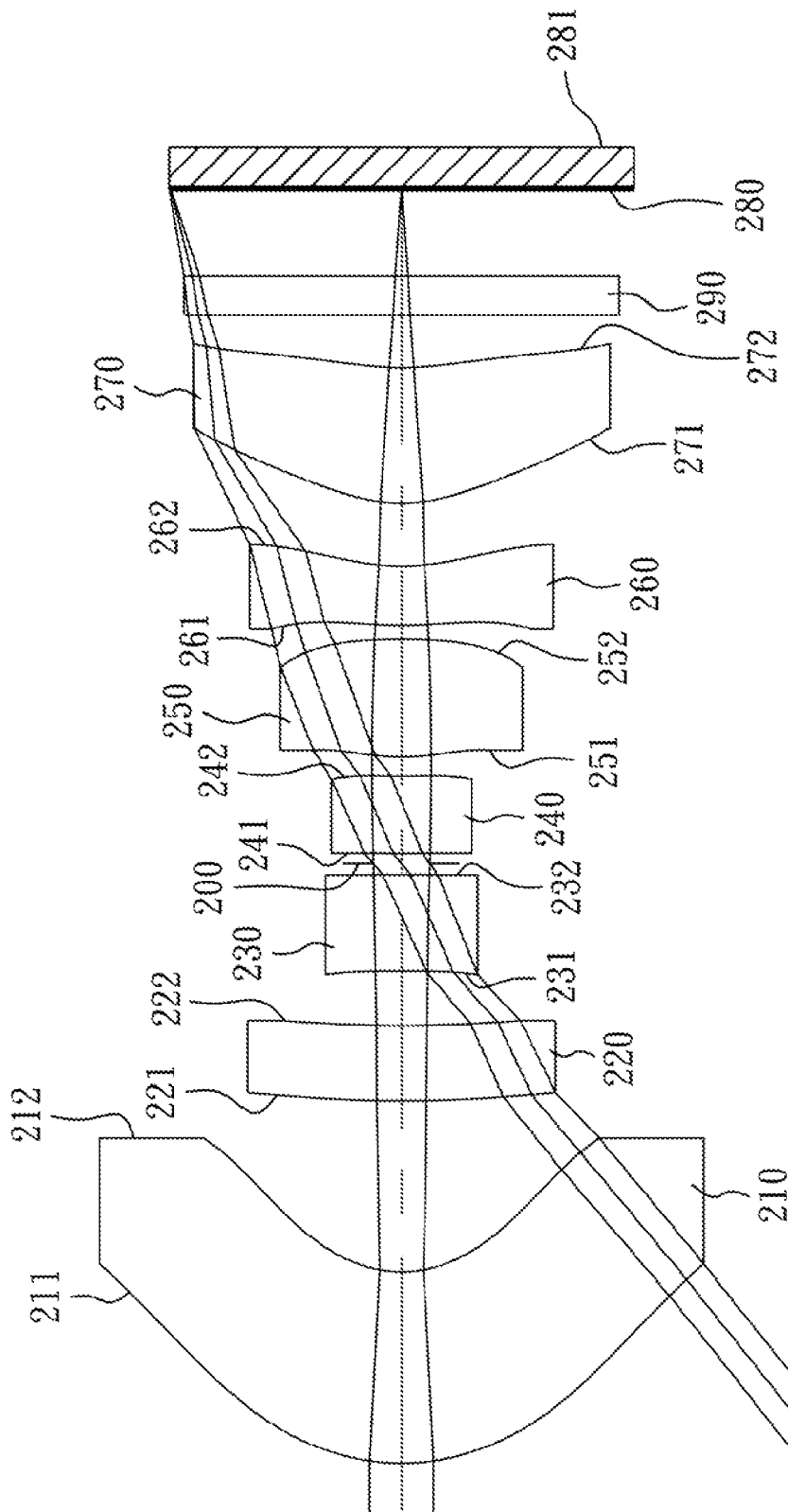


Fig. 3

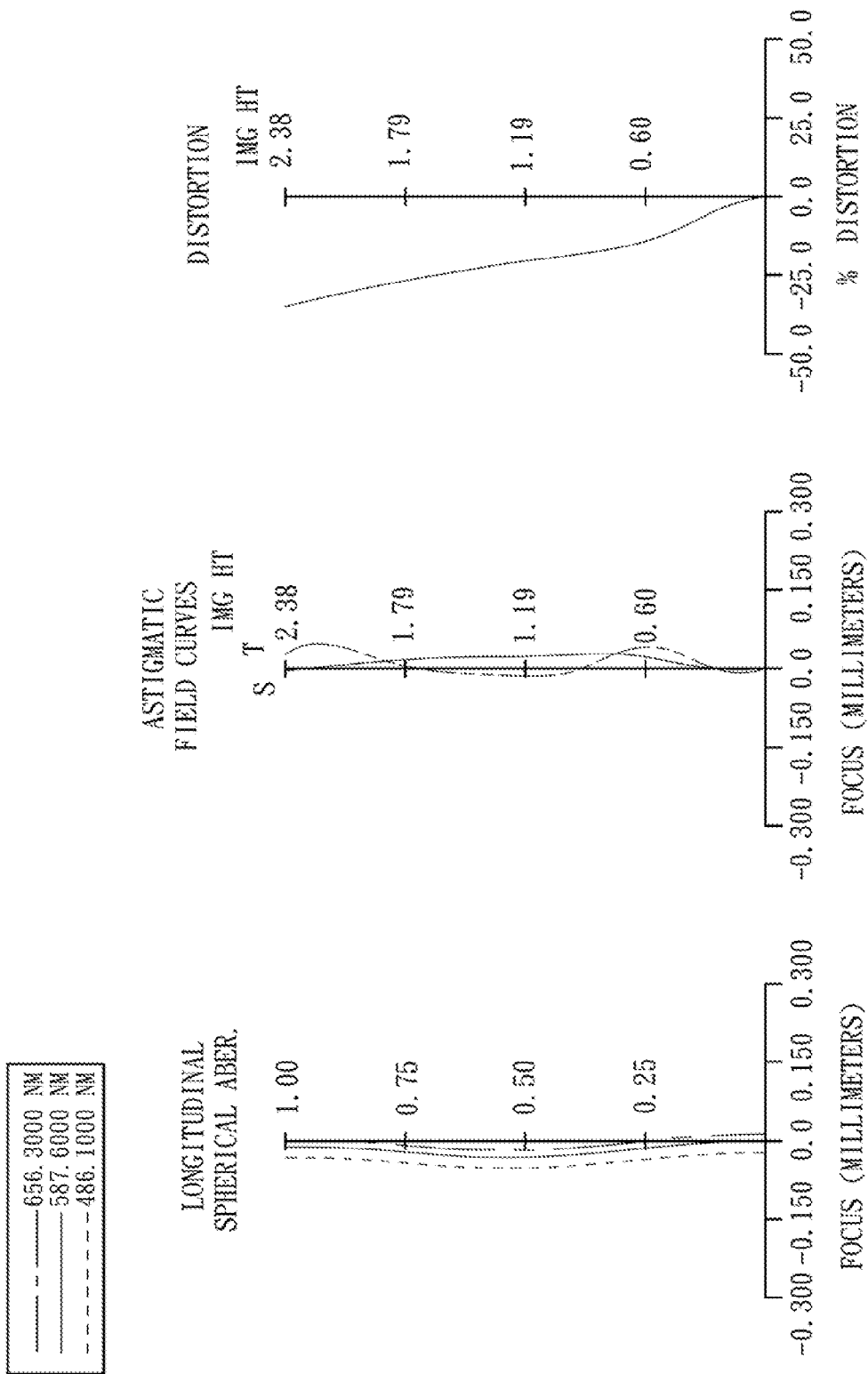


Fig. 4

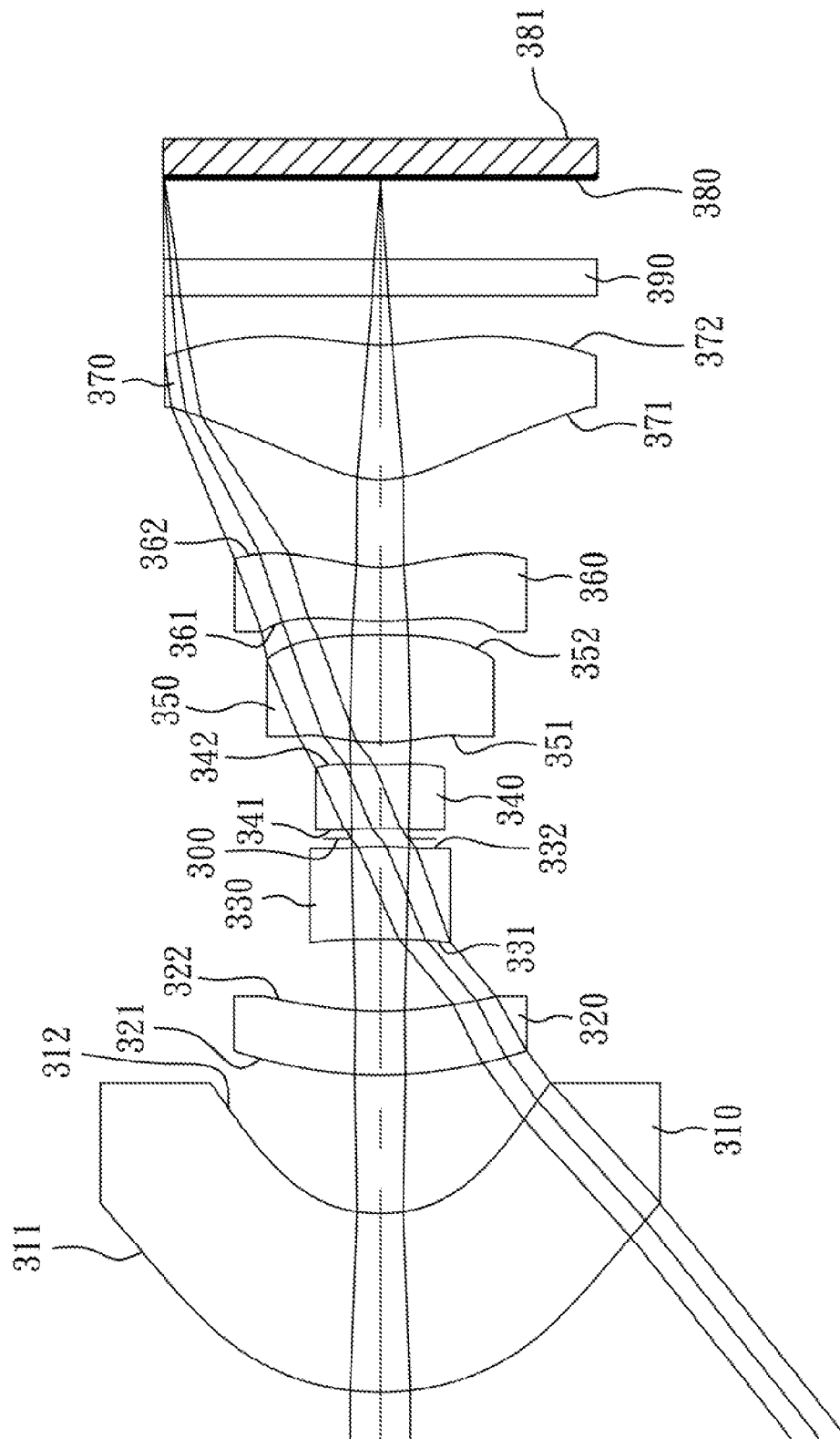
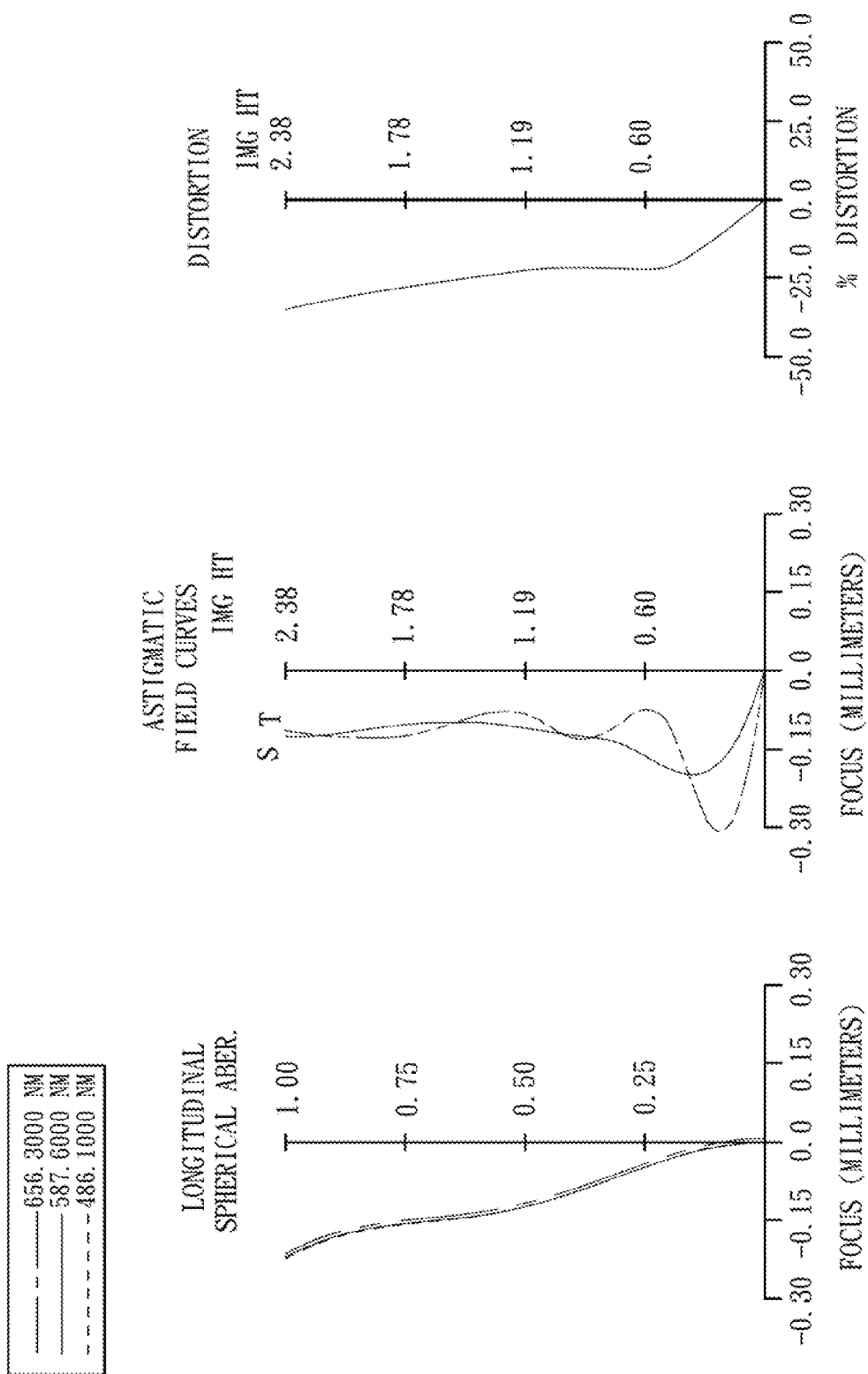


Fig. 5



60
61
62
63
64

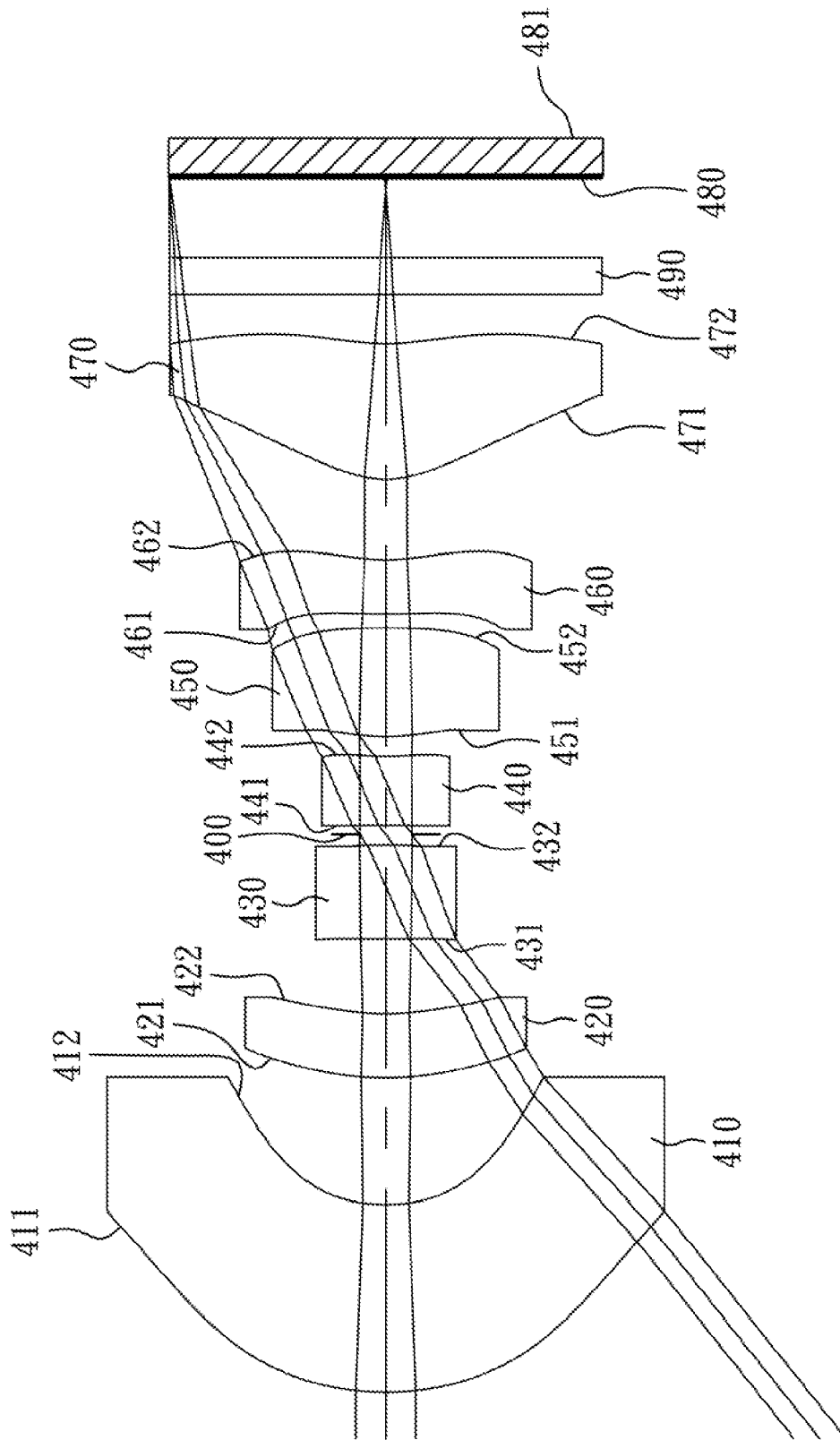
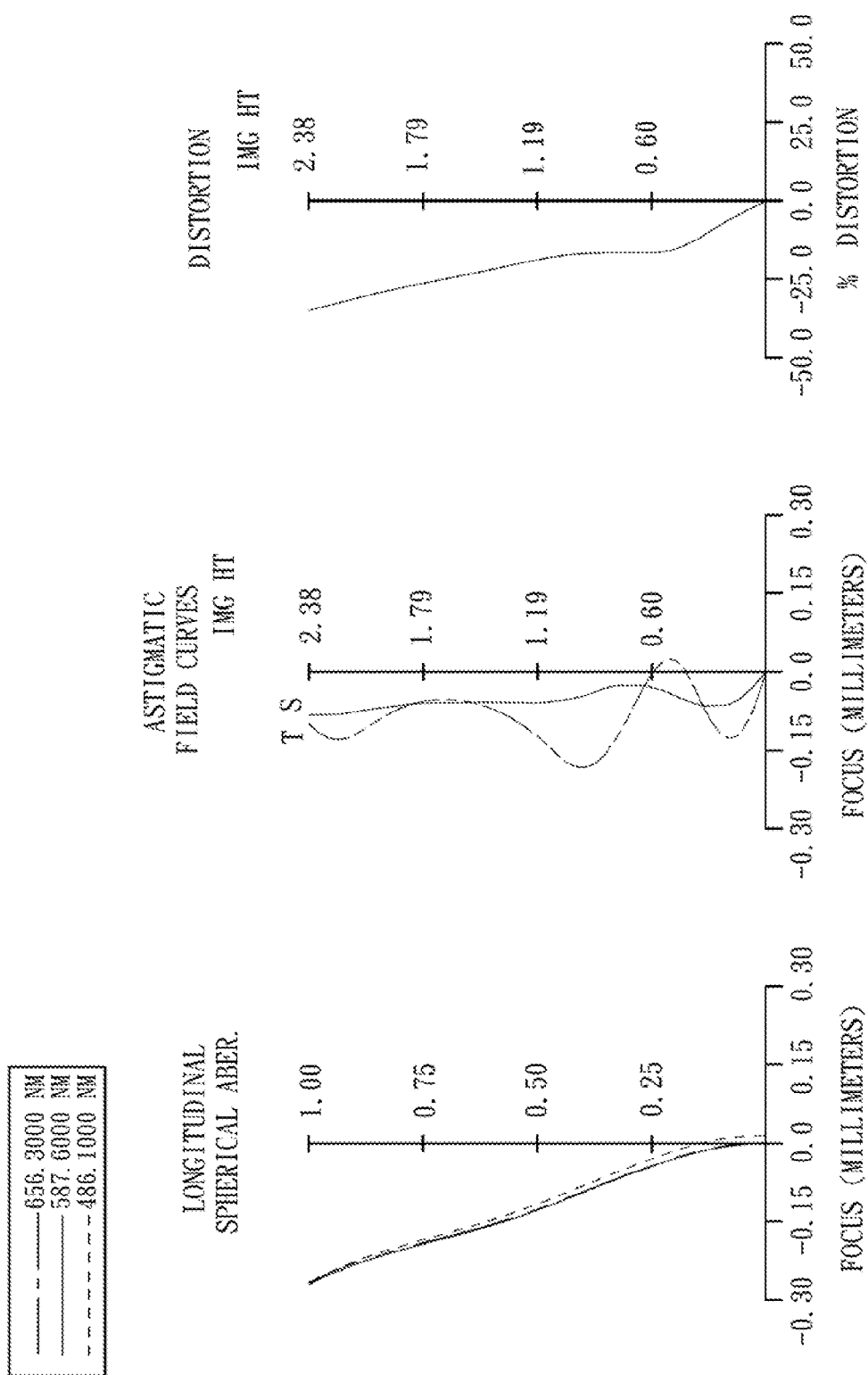


Fig. 7



∞
 $\frac{1}{2}$
 $\frac{1}{2}$
 $\frac{1}{2}$
 $\frac{1}{2}$

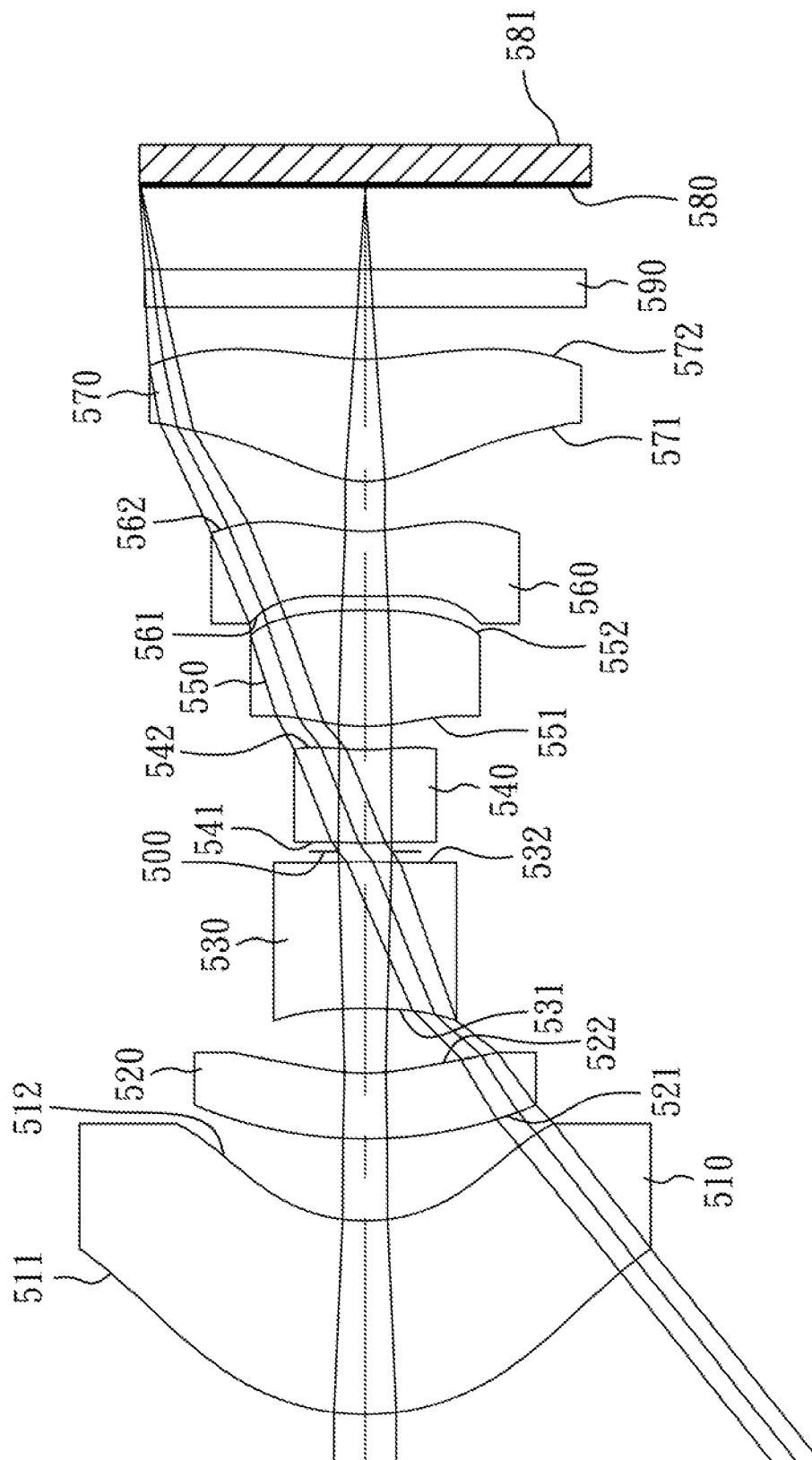


Fig. 9

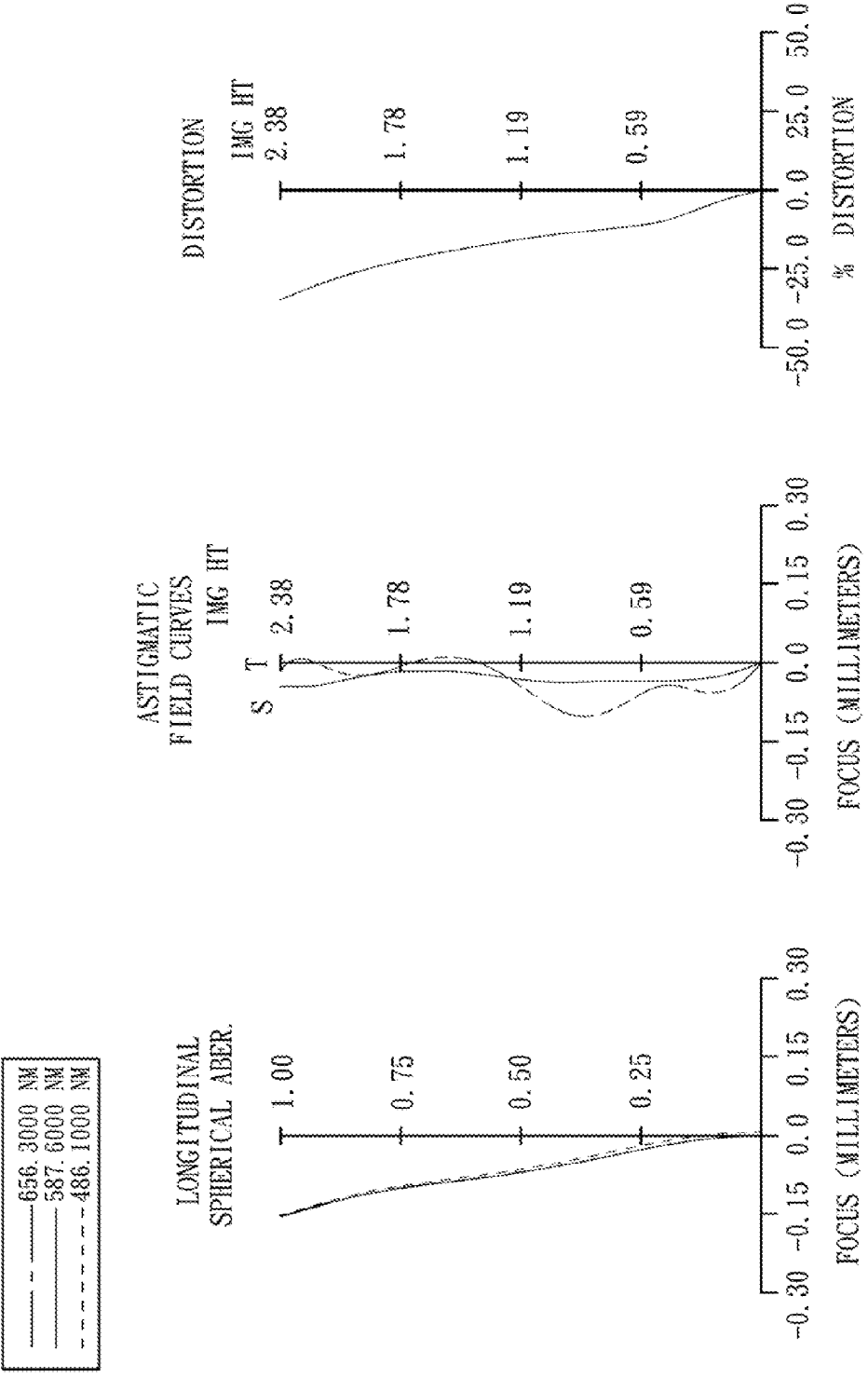


Fig. 10

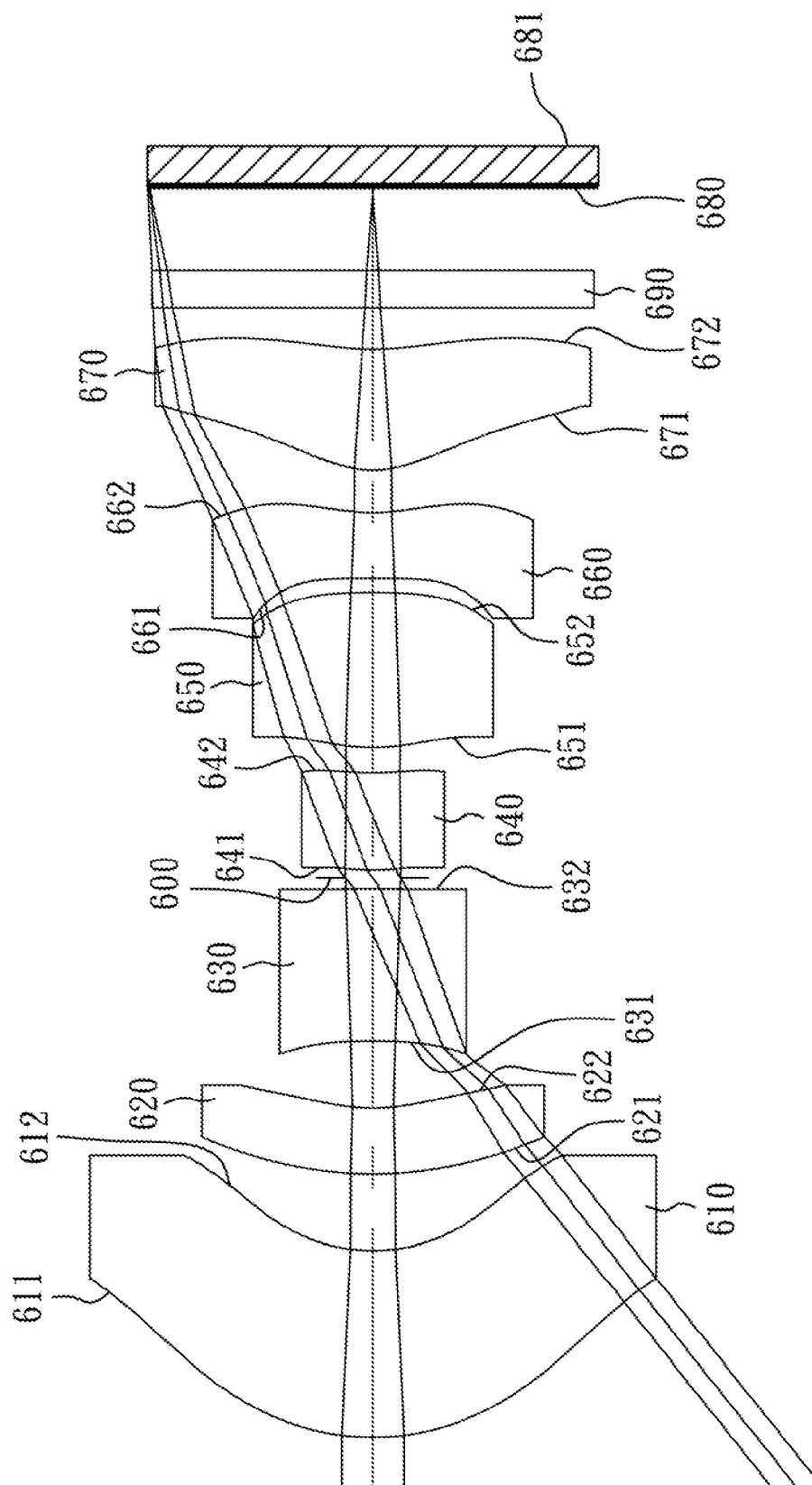


Fig. 11

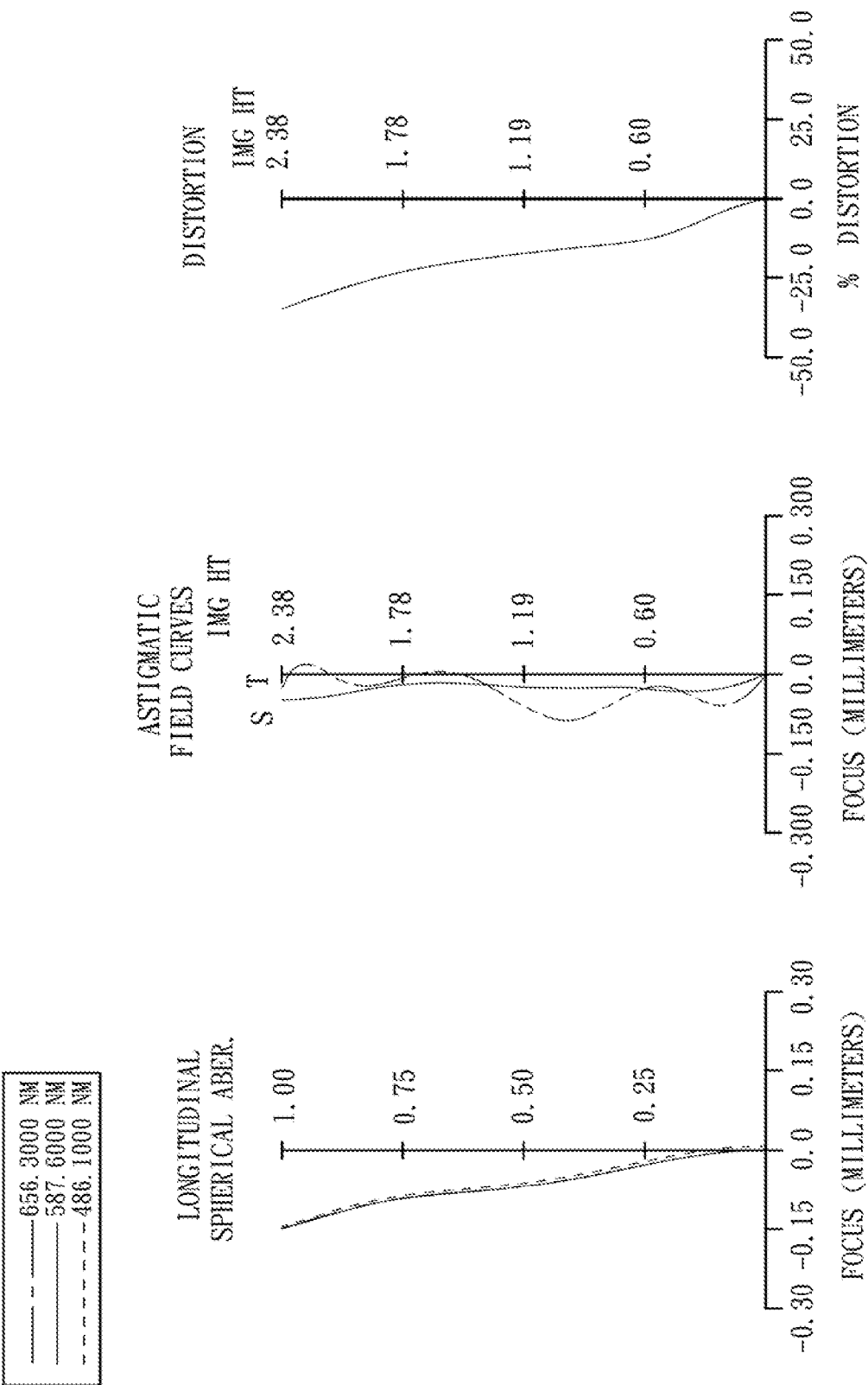
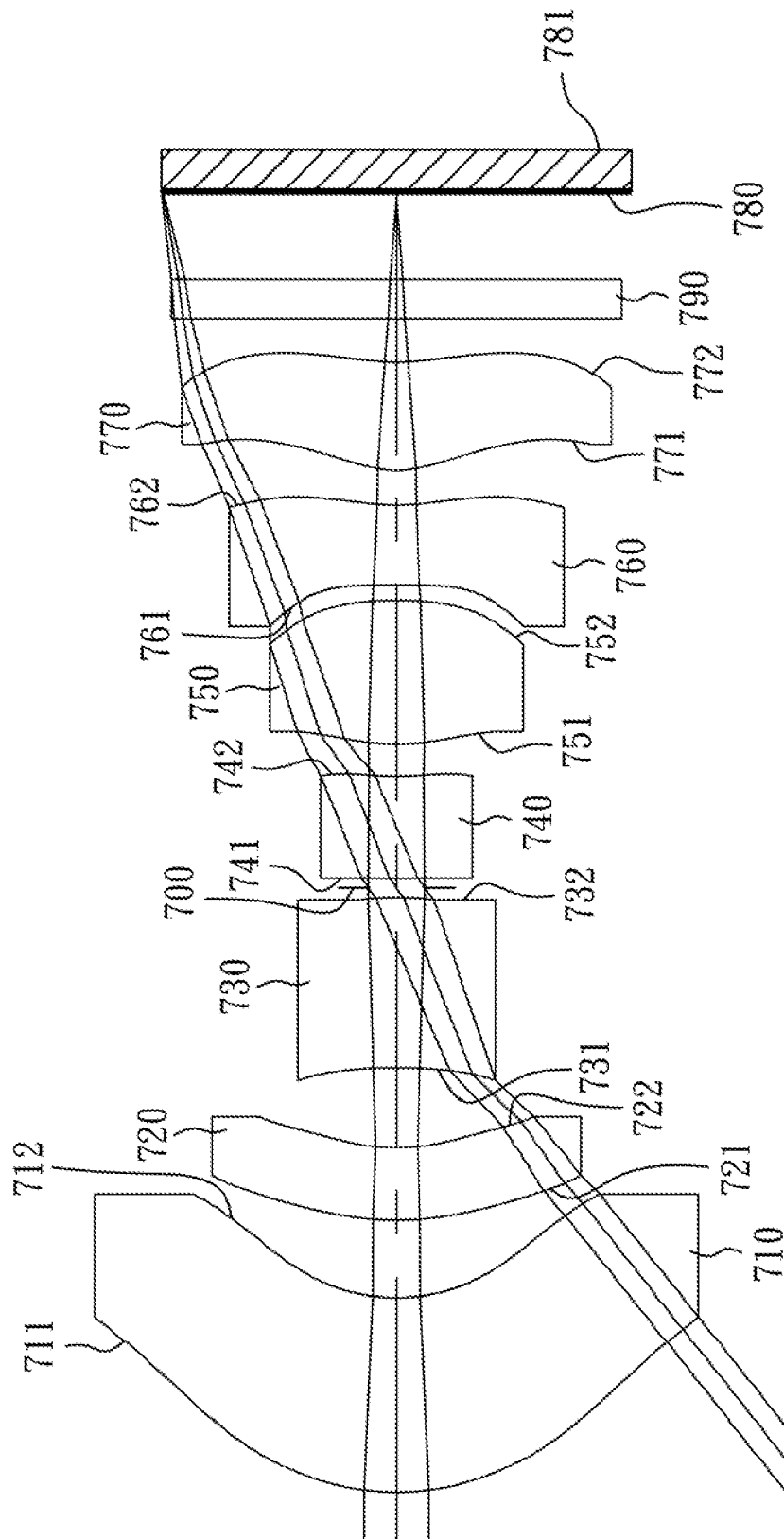


Fig. 12



30
b.0
a. 1000
L. 1000

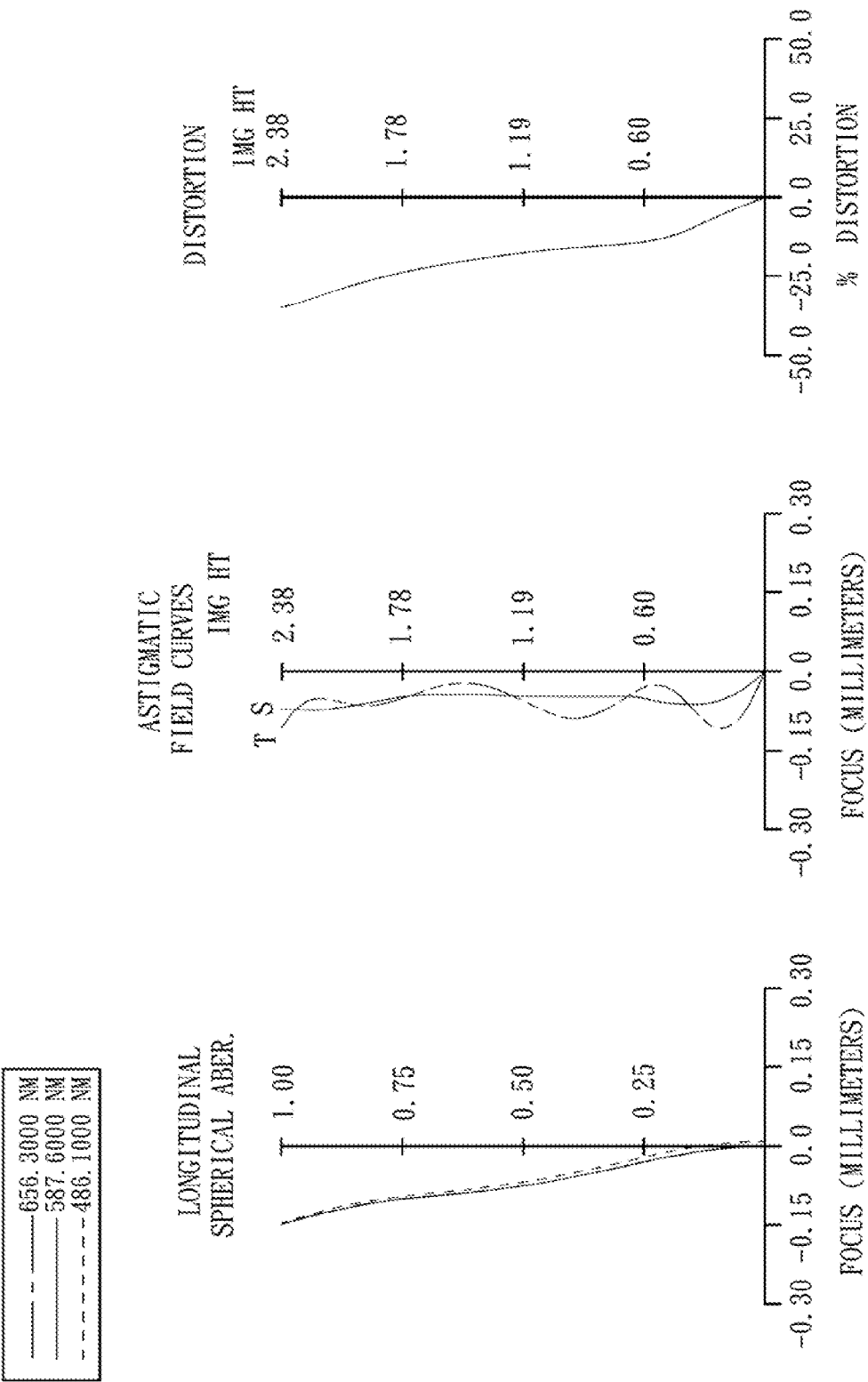


Fig. 14

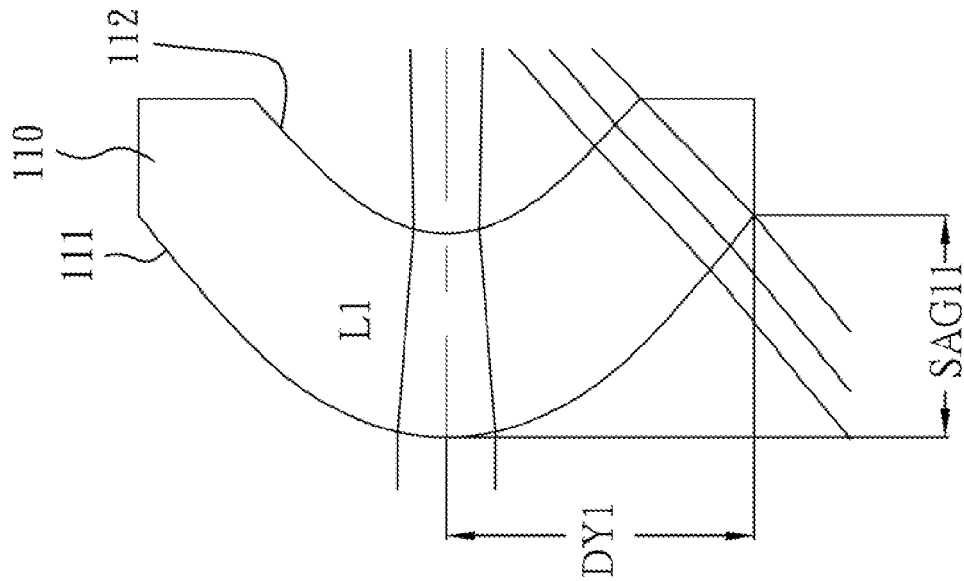


Fig. 15

OPTICAL IMAGE CAPTURING LENSES

RELATED APPLICATIONS

The present application is a continuation of the application serial number 13/404,001, filed Feb. 24, 2012, the entire contents of which are hereby incorporated herein by reference, which claims priority to Taiwan Application Serial Number 100130316, filed Aug. 24, 2011, all of which are herein incorporated by reference.

BACKGROUND

1. Technical Field

The present invention relates to an optical image capturing lenses. More particularly, the present invention relates to a compact optical image capturing lenses applicable to electronic products.

2. Description of Related Art

In recent years, with the popularity of mobile products with camera functionalities, the demand for miniaturizing an optical image capturing lenses is increasing. The sensor of a conventional photographing camera is typically a CCD (Charge Coupled Device) or a CMOS (Complementary Metal-Oxide Semiconductor Sensor). As advanced semiconductor manufacturing technologies have allowed the pixel size of sensors to be reduced and compact optical image capturing lenses have gradually evolved toward the fields of higher megapixels, there is an increasing demand for optical image capturing lenses featuring better image quality.

A conventional optical image capturing lenses in a portable electronic product typically utilizes a three-element lens structure. Such a conventional optical image capturing lenses has a first lens element with positive refractive power, a second lens element with negative refractive power and a third lens element with positive refractive power. The first, second and third lens elements are arranged in this order from an object-side to an image-side. Although the three-element lens structure is compact, it is not able to produce high quality images.

Further, another conventional compact optical image capturing lenses to provides a four-element lens structure. The first lens element and the second lens element of the four-element lens structure are two glass spherical lens elements which are attached to each other to form a doublet lens for eliminating chromatic aberration. However, this lens structure requires a longer total optical track length caused by insufficient degrees of freedom in setting system parameters due to too many spherical lenses allocated. Moreover, it is not easy to attach the glass lenses, and thus the manufacturing process for forming the glass doublet lenses is difficult. Therefore, a need exists in the art for providing an optical image capturing lenses for use in a mobile electronic product that has excellent imaging quality without too long total track length.

Moreover, the problem of the foregoing optical image capturing lenses is that both of the image quality and the production cost can not be maintained. In detail, two different lenses assemblies should be used when photographing a near object and a far object. However, the difficulty or the cost of the production would be increased by preparing two lenses assemblies or one lenses assembly which can be adjusted.

SUMMARY

According to one aspect of the present disclosure, an optical image capturing lenses includes, in order from an object

side to an image side, a first lens element, a second lens element, a third lens element, a fourth lens element, a fifth lens element and a sixth lens element. The first lens element with refractive power has a convex object-side surface and a concave image-side surface. The second lens element with negative refractive power has a convex object-side surface and a concave image-side surface. The third lens element has refractive power. The fourth lens element has positive refractive power. The fifth lens element with refractive power is made of plastic material, wherein an object-side surface and an image-side surface of the fifth lens element are aspheric. The sixth lens element with refractive power has a convex object-side surface and a concave image-side surface and is made of plastic material, wherein the object-side surface and the image-side surface of the sixth lens element are aspheric, and the image-side surface of the sixth lens element has at least one inflection point thereon. The optical image capturing lenses has a total of six lens elements with refractive power, wherein there is an air gap in a paraxial region between any two of the first lens element, the second lens element, the third lens element, the fourth lens element, the fifth lens element and the sixth lens element that are adjacent to each other.

According to another aspect of the present disclosure, an optical image capturing lenses includes, in order from an object side to an image side, a first lens element, a second lens element, a third lens element, a fourth lens element, a fifth lens element and a sixth lens element. The first lens element with refractive power has a convex object-side surface. The second lens element with refractive power has a convex object-side surface. The third lens element has refractive power. The fourth lens element has positive refractive power. The fifth lens element with refractive power is made of plastic material, wherein an object-side surface and an image-side surface of the fifth lens element are aspheric. The sixth lens element with positive refractive power has a convex object-side surface and a concave image-side surface and is made of plastic material, wherein the object-side surface and the image-side surface of the sixth lens element are aspheric, and the image-side surface of the sixth lens element has at least one inflection point thereon. The optical image capturing lenses has a total of six lens elements with refractive power, wherein there is an air gap in a paraxial region between any two of the first lens element, the second lens element, the third lens element, the fourth lens element, the fifth lens element and the sixth lens element that are adjacent to each other.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a schematic view of an optical image capturing lenses according to the first embodiment of the present disclosure;

FIG. 2 shows spherical aberration curves, astigmatic field curves and a distortion curve of the optical image capturing lenses according to the first embodiment;

FIG. 3 is a schematic view of an optical image capturing lenses according to the second embodiment of the present disclosure;

FIG. 4 shows spherical aberration curves, astigmatic field curves and a distortion curve of the optical image capturing lenses according to the second embodiment;

FIG. 5 is a schematic view of an optical image capturing lenses according to the third embodiment of the present disclosure;

FIG. 6 shows spherical aberration curves, astigmatic field curves and a distortion curve of the optical image capturing lenses according to the third embodiment;

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FIG. 7 is a schematic view of an optical image capturing lenses according to the fourth embodiment of the present disclosure;

FIG. 8 shows spherical aberration curves, astigmatic field curves and a distortion curve of the optical image capturing lenses according to the fourth embodiment;

FIG. 9 is a schematic view of an optical image capturing lenses according to the fifth embodiment of the present disclosure;

FIG. 10 shows spherical aberration curves, astigmatic field curves and a distortion curve of the optical image capturing lenses according to the fifth embodiment;

FIG. 11 is a schematic view of an optical image capturing lenses according to the sixth embodiment of the present disclosure;

FIG. 12 shows spherical aberration curves, astigmatic field curves and a distortion curve of the optical image capturing lenses according to the sixth embodiment;

FIG. 13 is a schematic view of an optical image capturing lenses according to the seventh embodiment of the present disclosure;

FIG. 14 shows spherical aberration curves, astigmatic field curves and a distortion curve of the optical image capturing lenses according to the seventh embodiment; and

FIG. 15 shows the incident light passing through the first lens element of the optical image capturing lenses according to the first embodiment.

DETAILED DESCRIPTION

An optical image capturing lenses includes, in order from an object side to an image side, a front lens group, a stop and a rear lens group. The optical image capturing lenses further includes an image sensor located on an image plane.

The front lens group includes, in order from an object side to an image side, at least a first lens element and a second lens element. The first lens element with refractive power has a convex object-side surface and a concave image-side surface. Therefore, the astigmatism of the optical image capturing lenses can be corrected for increasing the image quality. The second lens element has refractive power. The rear lens group includes, in order from an object side to an image side, at least a third lens element, a fourth lens element, a fifth lens element and a sixth lens element. The third lens element has refractive power. The fourth lens element with positive refractive power has a convex object-side surface and a convex image-side surface, so that the refractive of the fourth lens element can be enhanced and the total track length of the optical image capturing lenses can be reduced. The fifth lens element with negative refractive power has a convex object-side surface and a concave image-side surface, and is made of plastic material, wherein the object-side surface and the image-side surface of the fifth lens element are aspheric. Therefore, the aberration generated from the lens elements with positive refractive power can be corrected and the astigmatism of the optical image capturing lenses can also be corrected while increasing the image quality and decreasing the production cost effectively. The sixth lens element with positive refractive power has a convex object-side surface and a concave image-side surface, and is made of plastic material, wherein the object-side surface and the image-side surface of the sixth lens element are aspheric, and the sixth lens element has at least one inflection point formed on at least one of the object-side surface and the image-side surface thereof. Therefore, the incident angle of the off-axis field of light on the image sensor can be effectively minimized and the aberration of the off-axis field can be corrected. Furthermore, the sixth

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lens element can provide partial refractive power for reducing the total track length and the sensitivity of the optical image capturing lenses, so that the production cost can be reduced. At least three lens elements of the foregoing lens elements are made of plastic material, so that the production cost can be reduced. Moreover, the optical image capturing lenses can include seven lens elements with refractive power. When a maximal field of view of the optical image capturing lenses is FOV, a maximal negative distortion of the optical image capturing lenses is DIST, a maximal chief ray angle on an image plane of the optical image capturing lenses is CR_{Amax}, a focal length of the front lens group is *f*, a focal length of the rear lens group is *f_r*, the maximum SAG of the effective aperture on the object-side surface of the first lens element is SAG₁₁, an effective radius of the object-side surface of the first lens element is YD₁, a focal length of the optical image capturing lenses is *f*, a focal length of the first lens element is *f₁*, a central thickness of the first lens element is CT₁, a central thickness of the second lens element is CT₂, a curvature radius of an object-side surface of the lens element nearest to the image plane with negative refractive power is Rn₁, and a curvature radius of an image-side surface of the lens element nearest to the image plane with negative refractive power is Rn₂, the following relationships are satisfied:

$$55 \text{ degrees} < FOV < 90 \text{ degrees};$$

$$-70\% < DIST < -25\%; \text{ and}$$

$$CR_{Amax} < 15 \text{ degrees}.$$

Moreover, according to the different arrangement of the optical image capturing lenses of the present disclosure, the following relationships are satisfied:

$$-1.0 < f/r/f < 0.1;$$

$$-70\% < DIST < -30\%;$$

$$CR_{Amax} < 10 \text{ degrees};$$

$$-0.5 < f/r/f < -0.1;$$

$$0.3 < SAG_{11}/YD_1 < 1.0;$$

$$-0.6 < f/f_1 < 0.3;$$

$$0.5 < SAG_{11}/YD_1 < 0.8;$$

$$2.0 < CT_1/CT_2 < 3.5; \text{ and}$$

$$0 < (Rn_1 - Rn_2)/(Rn_1 + Rn_2) < 1.5.$$

According to another embodiment of the present disclosure, the optical image capturing lenses includes at least five lens elements. At least one lens element has at least one inflection point formed on at least one of an object-side surface and an image-side surface thereof, and is made of plastic material. The three lens elements respectively in order from the object side has positive, negative, and positive refractive power, so that the total track length and the sensitivity of the optical image capturing lenses can be reduced. The aberration generated from the lens elements with positive refractive power and the astigmatism of the optical image capturing lenses can be corrected by the lens element with negative refractive power. The lens element with negative refractive power has a convex object-side surface and a concave image-side surface and has at least one inflection point formed on at least one of the object-side surface and the image-side surface thereof. Therefore, the incident angle of the off-axis field of light on the image sensor can be effectively minimized and

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the aberration of the off-axis field can be corrected. The optical image capturing lenses includes, in order from an object side to an image side, a first lens element and a second lens element. The first lens element has a convex object-side surface and a concave image-side surface. The second lens element has a convex object-side surface and a concave image-side surface. Therefore, the astigmatism of the optical image capturing lenses can be corrected for increasing the image quality. When a maximal field of view of the optical image capturing lenses is FOV, a maximal negative distortion of the optical image capturing lenses is DIST, a maximal chief ray angle on an image plane of the optical image capturing lenses is CR_{Amax}, a focal length of the front lens group is ff, a focal length of the rear lens group is fr, a central thickness of the first lens element is CT₁, and a central thickness of the second lens element is CT₂, the following relationships are satisfied:

$$55 \text{ degrees} < FOV < 90 \text{ degrees};$$

$$-70\% < DIST < -25\%;$$

$$CR_{Amax} < 15 \text{ degrees}; \text{ and}$$

$$-0.5 < fr/ff < -0.1.$$

Moreover, according to the different arrangement of the optical image capturing lenses of the present disclosure, the following relationships are satisfied:

$$2.0 < CT_1/CT_2 < 3.5; \text{ and}$$

$$CR_{Amax} < 10 \text{ degrees}.$$

According to another embodiment of the present disclosure, the optical to image capturing lenses includes at least five lens elements. At least one lens element has at least one inflection point formed on at least one of an object-side surface and an image-side surface thereof, and is made of plastic material. Therefore, the incident angle of the off-axis field of light on the image sensor can be effectively minimized and the aberration of the off-axis field can be corrected. The lens element which is nearest to the object is the first lens element. The first lens element has a convex object-side surface and a concave image-side surface, so that the astigmatism of the optical image capturing lenses can be corrected while increasing the image quality. The lens element which is nearest to the image plane has positive refractive power has a convex object-side surface and a concave image-side surface, and has at least one inflection point formed on at least one of the object-side surface and the image-side surface thereof. Therefore, the incident angle of the off-axis field of light on the image sensor can be effectively minimized and the aberration of the off-axis field can be corrected, and the astigmatism also can be corrected for increasing the image quality. The optical image capturing lenses includes, in order from an object side to an image side, the first lens element and the second lens element, wherein the second lens element has a convex object-side surface and a concave image-side surface. Therefore, the astigmatism of the optical image capturing lenses also can be corrected for increasing the image quality. When a maximal field of view of the optical image capturing lenses is FOV, a maximal negative distortion of the optical image capturing lenses is DIST, a maximal chief ray angle on an image plane of the optical image capturing lenses is CR_{Amax}, the maximum SAG of the effective aperture on the object-side surface of the first lens element is SAG₁₁, to and an effective radius of the object-side surface of the first lens element is YD₁, the following relationships are satisfied:

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$$55 \text{ degrees} < FOV < 90 \text{ degrees};$$

$$-70\% < DIST < -25\%;$$

$$CR_{Amax} < 15 \text{ degrees}; \text{ and}$$

$$0.3 < SAG_{11}/YD_1 < 1.0.$$

Moreover, according to the different arrangement of the optical image capturing lenses of the present disclosure, the following relationships are satisfied:

$$0 < (Rn_1 - Rn_2)/(Rn_1 + Rn_2) < 1.5; \text{ and}$$

$$70 \text{ degrees} < FOV < 80 \text{ degrees}.$$

According to yet another embodiment of the present disclosure, the front lens group includes, in order from an object side to an image side, a first lens element, a second lens element and a third lens element. The first lens element with refractive power has a convex object-side surface and a concave image-side surface, so that the astigmatism of the optical image capturing lenses can be corrected for increasing the image quality. The second lens element has refractive power. The third lens element has refractive power. The rear lens group includes, in order from an object side to an image side, a fourth lens element, a fifth lens element, a sixth lens element and a seventh lens element. The fourth lens element has refractive power. The fifth lens element with positive refractive power has a convex object-side surface and a convex image-side surface, so that the refractive power thereof can be enhanced and the total track length of the optical image capturing lenses can be reduced. The sixth lens element with negative refractive power has a convex object-side surface and a concave image-side surface, and is made of plastic material, wherein the object-side surface and the image-side surface of the sixth lens element are aspheric. Therefore, the aberration generated from the lens elements with positive refractive power and the astigmatism of the optical image capturing lenses can be corrected for increasing the image quality. The seventh lens element with positive refractive power has a convex object-side surface and a concave image-side surface, and is made of plastic material, wherein the object-side surface and the image-side surface of the seventh lens element are aspheric, and the seventh lens element has at least one inflection point formed on at least one of the object-side surface and the image-side surface thereof. Therefore, the incident angle of the off-axis field of light on the image sensor can be effectively minimized and the aberration of the off-axis field can be corrected, and the aberration and the sensitivity also can be corrected for increasing the image quality. When a maximal field of view of the optical image capturing lenses is FOV, a maximal negative distortion of the optical image capturing lenses is DIST, a focal length of the optical image capturing lenses is f, and a focal length of the first lens element is f₁, the following relationships are satisfied:

$$55 \text{ degrees} < FOV < 90 \text{ degrees}; \text{ and}$$

$$-70\% < DIST < -25\%.$$

Moreover, according to the different arrangement of the optical image capturing lenses of the present disclosure, the following relationships are satisfied:

$$CR_{Amax} < 15 \text{ degrees}; \text{ and}$$

$$-0.6 < f/f_1 < 0.3.$$

When FOV satisfies the foregoing relationship, the angle of view of the optical image capturing lenses is proper.

When DIST satisfies the foregoing relationship, the distortion and the aberration of the image are proper for satisfying the digital zoom function of the optical image capturing lenses.

When both of FOV and DIST satisfy the foregoing relationships, the optical image capturing lenses has good digital zoom effect for increasing the image quality of digital zoom.

When CRMax satisfies the foregoing relationship, the images from the far side and the near side can be better focused simultaneously. When f/f' satisfies the foregoing relationship, the ratio of the focal length of the front lens group and the focal length of the rear lens group is proper for increasing the field of view, so that the wide-angle function of the optical image capturing lenses can be improved, and the total track length of the optical image capturing lenses is proper.

When SAG11/YD1 satisfies the foregoing relationship, the refractive power of the first lens element is proper which can increase the field of view, so that the wide-angle function of the optical image capturing lenses can be improved.

When f/f_1 satisfies the foregoing relationship, the field of view can be increased, so that the wide-angle function of the optical image capturing lenses can be improved.

When CT1/CT2 satisfies the foregoing relationship, the thicknesses of the first lens element and the second lens element are proper, so that the total to track length can be reduced, the manufacture of the lens elements is easier and the yield of the manufacture can be increased.

According to the optical image capturing lenses of the present disclosure, the lens elements thereof can be made of plastic material or glass. When the lens elements are made of plastic material, the cost of manufacture can be effectively reduced. When the lens elements are made of glass material, the range of the refractive power of the optical image capturing lenses can be set may be increased.

Furthermore, the surface of each lens element can be aspheric, so that it is easier to make the surface into non-spherical shapes. As a result, more controllable variables are obtained, and the aberration is reduced, and the number of required lens elements can be reduced while constructing an optical system. Therefore, the total track length of the optical image capturing lenses can also be reduced.

According to the optical image capturing lenses of the present disclosure, the optical image capturing lenses can include at least one stop, may it be glare stop or field stop, for reducing stray light while retaining high image quality.

Furthermore, when the stop is an aperture stop, the position of the aperture stop within an optical system can be arbitrarily placed in front of the entire optical system, within the optical system, including in front of the image plane, in accordance with the preference of the designer of the optical system, in order to achieve the desirable optical features or higher image quality produced from the optical system.

The optical image capturing lenses of the present disclosure can retain high image quality when far shooting or near shooting. Moreover, the image to plane can be moved when changing the mode (far side shooting or near side shooting), so that the optical image capturing lenses does not need to set two lens group for far shooting and near shooting.

According to the above description of the present disclosure, the following 1st-7th specific embodiments are provided for further explanation.

FIG. 1 is a schematic view of an optical image capturing lenses according to the first embodiment of the present disclosure. FIG. 2 shows spherical aberration curves, astigmatic field curves and a distortion curve of the optical image capturing lenses according to the first embodiment. In FIG. 1, the

optical image capturing lenses includes, in order from an object side to an image side, the first lens element 110, the second lens element 120, an aperture stop 100, the third lens element 130, the fourth lens element 140, the fifth lens element 150, the sixth lens element 160, an IR (infrared) cut filter 180, an image plane 170 and an image sensor 171. The first lens element 110 and the second lens element 120 belong to a front lens group. The third lens element, the fourth lens element, the fifth lens element and the sixth lens element belong to a rear lens group.

The first lens element 110 with negative refractive power has a convex object-side surface 111 and a concave image-side surface 112, and is made of plastic material. The object-side surface 111 and the image-side surface 112 of the first lens element 110 are aspheric.

The second lens element 120 with negative refractive power has a convex object-side surface 121 and a concave image-side surface 122, and is made of plastic material. The object-side surface 121 and the image-side to surface 122 of the second lens element 120 are aspheric.

The third lens element 130 with positive refractive power has a convex object-side surface 131 and a concave image-side surface 132, and is made of plastic material. The object-side surface 131 and the image-side surface 132 of the third lens element 130 are aspheric.

The fourth lens element 140 with positive refractive power has a convex object-side surface 141 and a convex image-side surface 142, and is made of plastic material. The object-side surface 141 and the image-side surface 142 of the fourth lens element 140 are aspheric. Moreover, the fourth lens element 140 has inflection points formed on the object-side surface 141 thereof. The fifth lens element 150 with negative refractive power has a convex object-side surface 151 and a concave image-side surface 152, and is made of plastic material. The object-side surface 151 and the image-side surface 152 of the fifth lens element 150 are aspheric. Moreover, the fifth lens element 150 has inflection points formed on the object-side surface 151 and the image-side surface 152 thereof.

The sixth lens element 160 with positive refractive power has a convex object-side surface 161 and a concave image-side surface 162, and is made of plastic material. The object-side surface 161 and the image-side surface 162 of the sixth lens element 160 are aspheric. Moreover, the sixth lens element 160 has inflection points formed on the object-side surface 161 and the image-side surface 162 thereof.

The IR cut filter 180 is made of glass and located between the sixth lens element 160 and the image plane 170, and will not affect the focal length of the optical image capturing lenses.

The equation of the aspheric surface profiles of the aforementioned lens elements of the first embodiment is expressed as follows:

$$X(Y) = (Y^2/R)/(1 + \sqrt{1 - (1+k) \times (Y/R)^2}) + \sum_i (Ai) \times (Y^i)$$

where:

X is the distance of a point on the aspheric surface spaced at a distance Y from the optical axis relative to the tangential plane at the aspheric surface vertex;

Y is the distance from the point on the curve of the aspheric surface to the optical axis;

R is the curvature radius of the lens elements;

k is the conic coefficient; and

Ai is the i-th aspheric coefficient.

In the optical image capturing lenses according to the first embodiment, when a focal length of the optical image capturing lenses is f , an f -number of the optical image capturing lenses is Fno , a half of the maximal field of view is $HFOV$, and a maximal field of view of the optical image capturing lenses is FOV , these parameters have the following values:

$f=5.72$ mm;
 $Fno=6.00$;
 $HFOV=39.5$ degrees; and
 $FOV=79$ degrees.

In the optical image capturing lenses according to the first embodiment, when a central thickness of the first lens element **110** is $CT1$, and a central thickness of the second lens element **120** is $CT2$, the following relationship is to satisfied:

$$CT1/CT2=2.86.$$

In the optical image capturing lenses according to the first embodiment, the lens element which is nearest to the image plane **170** and has negative refractive power is the fifth lens element **150**, when a curvature radius of an object-side surface **151** thereof is $Rn1$, and a curvature radius of an image-side surface **152** thereof is $Rn2$, the following relationship is satisfied:

$$(Rn1-Rn2)/(Rn1+Rn2)=0.17.$$

In the optical image capturing lenses according to the first embodiment, when a focal length of the optical image capturing lenses is f , and a focal length of the first lens element **110** is $f1$, the following relationship is satisfied:

$$f/f1=-0.23.$$

In the optical image capturing lenses according to the first embodiment, when a focal length of the front lens group is f_f , and a focal length of the rear lens group is f_r , the following relationship is satisfied:

$$f_r/f_f=-0.28.$$

In the optical image capturing lenses according to the first embodiment, when a maximal chief ray angle on an image plane **170** of the optical image capturing lenses is CRA_{max} , wherein the chief ray pass through the center of the aperture stop **100** from the off-axis point, the following relationship is satisfied:

$$CRA_{max}=14.6 \text{ degrees.}$$

In the optical image capturing lenses according to the first embodiment, when a maximal negative distortion of the optical image capturing lenses is $DIST$, the following relationship is satisfied:

$$DIST=-39.0\%.$$

FIG. **15** shows the incident light passing through the first lens element **110** of the optical image capturing lenses according to the first embodiment. In FIG. **15**, the maximum SAG of the effective aperture on the object-side surface **111** of the first lens element **110** is $SAG11$. In other word, a horizontal distance from the position of the maximum range of the incident light which passing through the object-side surface **111** of the first lens element **110** to the vertex of the object-side surface **111** of the first lens element **110** is $SAG11$ on the optical axis, and an effective radius of the object-side surface **111** of the first lens element **110** is $YD1$, the following relationship is satisfied:

$$SAG11/YD1=0.72.$$

The detailed optical data of the first embodiment are shown in Table 1 and the aspheric surface data are shown in Table 2 below.

TABLE 1

| 1st Embodiment | | | | | | | |
|--|-----------|------------------|-----------|----------|-------|--------|--------------|
| $f = 5.72$ mm, $Fno = 6.00$, $HFOV = 39.5$ deg. | | | | | | | |
| Surface # | | Curvature Radius | Thickness | Material | Index | Abbe # | Focal length |
| 0 | Object | Plano | Infinity | | | | |
| 1 | Lens 1 | 2.086509 (ASP) | 2.000 | Plastic | 1.535 | 56.3 | -25.41 |
| 2 | | 1.204756 (ASP) | 2.410 | | | | |
| 3 | Lens 2 | 6.331207 (ASP) | 0.700 | Plastic | 1.650 | 21.4 | -15.30 |
| 4 | | 3.699331 (ASP) | 0.128 | | | | |
| 5 | Ape. Stop | Plano | 0.090 | | | | |
| 6 | Lens 3 | 10.808304 (ASP) | 1.194 | Plastic | 1.544 | 55.9 | 27.34 |
| 7 | | 37.984310 (ASP) | 0.310 | | | | |
| 8 | Lens 4 | 2.448117 (ASP) | 1.348 | Plastic | 1.544 | 55.9 | 3.76 |
| 9 | | -10.092182 (ASP) | 0.150 | | | | |
| 10 | Lens 5 | 3.081457 (ASP) | 0.633 | Plastic | 1.650 | 21.4 | -16.50 |
| 11 | | 2.199585 (ASP) | 0.941 | | | | |
| 12 | Lens 6 | 2.348031 (ASP) | 1.058 | Plastic | 1.544 | 55.9 | 20.96 |
| 13 | | 2.487015 (ASP) | 0.550 | | | | |
| 14 | IR-filter | Plano | 0.400 | Glass | 1.517 | 64.2 | — |
| 15 | | Plano | 0.911 | | | | |
| 16 | Image | Plano | — | | | | |

Note:

Reference wavelength (d-line) is 587.6 nm.

TABLE 2

| Aspheric Coefficients | | | | | | |
|-----------------------|--------------|--------------|--------------|-------------|--------------|--------------|
| Surface # | 1 | 2 | 3 | 4 | 6 | 7 |
| k = | -9.33090E-01 | -2.83665E+00 | 1.57309E+01 | 2.46630E+01 | -5.00000E+01 | -5.00000E+01 |
| A4 = | -2.21243E-03 | 1.05200E-01 | -1.30840E-02 | 1.10753E-02 | 6.52771E-02 | -1.35568E-01 |

TABLE 2-continued

| Aspheric Coefficients | | | | | | |
|-----------------------|--------------|--------------|--------------|--------------|--------------|--------------|
| A6 = | 2.12556E-03 | -2.77844E-02 | -2.36645E-02 | -3.12519E-01 | -4.51043E-01 | 5.60962E-02 |
| A8 = | -3.87318E-04 | 2.08808E-03 | -7.59805E-03 | 6.59350E-01 | 2.02606E+00 | -4.27656E-02 |
| A10 = | 1.86880E-05 | 1.67973E-05 | 7.30841E-03 | -7.45752E-01 | -3.53581E+00 | 7.56635E-03 |
| Surface # | 8 | 9 | 10 | 11 | 12 | 13 |
| k = | -7.24415E+00 | -1.41792E+01 | -9.18189E+00 | -9.13512E+00 | -1.68561E+01 | -4.47258E+01 |
| A4 = | -4.52663E-02 | -7.70699E-02 | -6.29945E-02 | -9.63288E-03 | -1.16422E-02 | -6.21272E-03 |
| A6 = | 6.73989E-03 | 1.44426E-02 | 7.32922E-03 | 1.90708E-03 | 3.51857E-04 | -2.70674E-03 |
| A8 = | -5.40128E-03 | -5.90824E-04 | 2.76823E-03 | 2.71157E-05 | 3.38277E-04 | 3.98475E-04 |
| A10 = | | | -5.80205E-04 | -4.38230E-05 | -3.60586E-05 | -7.38041E-06 |
| A12 = | | | | | -2.78886E-07 | -1.53930E-06 |

In Table 1, the curvature radius, the thickness and the focal length are shown in millimeters (mm). Surface numbers **0-16** represent the surfaces sequentially arranged from the object-side to the image-side along the optical axis. In Table 2, *k* represents the conic coefficient of the equation of the aspheric surface profiles. **A1-A12** represent the aspheric coefficients ranging from the 1st order to the 12th order. This information related to Table 1 and Table 2 applies also to the Tables for the remaining embodiments, and thus an explanation in this regard will not be provided again.

FIG. 3 is a schematic view of an optical image capturing lenses according to the second embodiment of the present disclosure. FIG. 4 shows spherical aberration curves, astigmatic field curves and a distortion curve of the optical image capturing lenses according to the second embodiment. In FIG. 3, the optical image capturing lenses includes, in order from an object side to an image side, the first lens element **210**, the second lens element **220**, the third lens element **230**, an aperture stop **200**, the fourth lens element **240**, the fifth lens element **250**, the sixth lens element **260**, the seventh lens element **270**, an IR cut filter **290**, an image plane **280** and an image sensor **281**. The first lens element **210**, the second lens element **220** and the third lens element **230** belong to a front lens group. The fourth lens element **240**, the fifth lens element **250**, the sixth lens element **260** and the seventh lens element **270** belong to a rear lens group.

The first lens element **210** with negative refractive power has a convex object-side surface **211** and a concave image-side surface **212**, and is made of plastic material. The object-side surface **211** and the image-side surface **212** of the first lens element **210** are aspheric.

The second lens element **220** with negative refractive power has a convex object-side surface **221** and a concave image-side surface **222**, and is made of plastic material. The object-side surface **221** and the image-side surface **222** of the second lens element **220** are aspheric.

The third lens element **230** with negative refractive power has a concave object-side surface **231** and a concave image-side surface **232**, and is made of plastic material. The object-side surface **231** and the image-side surface **232** of the third lens element **230** are aspheric.

The fourth lens element **240** with negative refractive power has a convex object-side surface **241** and a concave image-side surface **242**, and is made of plastic material. The object-side surface **241** and the image-side surface **242** of the fourth lens element **240** are aspheric.

The fifth lens element **250** with positive refractive power has a convex object-side surface **251** and a convex image-side surface **252**, and is made of plastic material. The object-side surface **251** and the image-side surface **252** of the fifth lens element **250** are aspheric. Moreover, the fifth lens element **250** has inflection points formed on the object-side surface **251** thereof.

The sixth lens element **260** with negative refractive power has a convex object-side surface **261** and a concave image-side surface **262**, and is made of plastic material. The object-side surface **261** and the image-side surface **262** of the sixth lens element **260** are aspheric. Moreover, the sixth lens element **260** has inflection points formed on the object-side surface **261** and the image-side surface **262** thereof.

The seventh lens element **270** with positive refractive power has a convex object-side surface **271** and a concave image-side surface **272**, and is made of plastic material. The object-side surface **271** and the image-side surface **272** of the seventh lens element **270** are aspheric. Moreover, the seventh lens element **270** has inflection points formed on the image-side surface **272** thereof.

The IR cut filter **290** is made of glass and located between the seventh lens element **270** and the image plane **280**, and will not affect the focal length of the optical image capturing lenses.

The detailed optical data of the second embodiment are shown in Table 3 and the aspheric surface data are shown in Table 4 below.

TABLE 3

| 2nd Embodiment | | | | | | | |
|---|--------|------------------|-----------|----------|-------|--------|--------------|
| f = 4.61 mm, Fno = 7.00, HFOV = 38.5 deg. | | | | | | | |
| Surface # | | Curvature Radius | Thickness | Material | Index | Abbe # | Focal length |
| 0 | Object | Plano | Infinity | | | | |
| 1 | Lens 1 | 2.206160 (ASP) | 1.973 | Plastic | 1.544 | 55.9 | -19.74 |
| 2 | | 1.253346 (ASP) | 1.768 | | | | |
| 3 | Lens 2 | 14.477784 (ASP) | 0.769 | Plastic | 1.650 | 21.4 | -99.08 |
| 4 | | 11.572322 (ASP) | 0.568 | | | | |
| 5 | Lens 3 | -41.409680 (ASP) | 0.992 | Plastic | 1.535 | 56.3 | -37.72 |
| 6 | | 39.630857 (ASP) | 0.114 | | | | |

TABLE 3-continued

| 2nd Embodiment f = 4.61 mm, Fno = 7.00, HFOV = 38.5 deg. | | | | | | | |
|---|-----------|------------------|-----------|----------|-------|--------|--------------|
| Surface # | | Curvature Radius | Thickness | Material | Index | Abbe # | Focal length |
| 7 | Ape. Stop | Plano | 0.107 | | | | |
| 8 | Lens 4 | 13.978532 (ASP) | 0.788 | Plastic | 1.544 | 55.9 | -186.80 |
| 9 | | 12.044478 (ASP) | 0.207 | | | | |
| 10 | Lens 5 | 2.424643 (ASP) | 1.206 | Plastic | 1.544 | 55.9 | 3.58 |
| 11 | | -8.127308 (ASP) | 0.150 | | | | |
| 12 | Lens 6 | 4.298053 (ASP) | 0.600 | Plastic | 1.650 | 21.4 | -5.94 |
| 13 | | 1.921967 (ASP) | 0.647 | | | | |
| 14 | Lens 7 | 1.433808 (ASP) | 1.400 | Plastic | 1.544 | 55.9 | 4.58 |
| 15 | | 2.212476 (ASP) | 0.550 | | | | |
| 16 | IR-filter | Plano | 0.400 | Glass | 1.517 | 64.2 | — |
| 17 | | Plano | 0.904 | | | | |
| 18 | Image | Plano | — | | | | |

Note: Reference wavelength (d-line) is 587.6 nm.

TABLE 4

| Aspheric Coefficients | | | | | | | |
|-----------------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|
| Surface # | 1 | 2 | 3 | 4 | 5 | 6 | 8 |
| k = | -8.80549E-01 | -2.13593E+00 | 2.36465E+01 | -1.72132E+01 | 5.00000E+01 | -1.00000E+02 | 5.00000E+01 |
| A4 = | -1.73797E-03 | 9.54804E-02 | 1.34980E-03 | -7.11759E-03 | -8.89742E-02 | -1.48314E-01 | -3.13903E-02 |
| A6 = | 1.98684E-03 | -2.84402E-02 | -2.46154E-04 | -1.03894E-03 | -7.98074E-03 | -8.84638E-02 | -2.03299E+00 |
| A8 = | -3.90415E-04 | 2.24684E-03 | -3.86078E-04 | 1.43932E-03 | 5.16887E-02 | 6.42000E-01 | 1.53431E+01 |
| A10 = | 1.77097E-05 | -3.23989E-06 | | | -2.66000E-02 | -1.35568E+00 | -4.29502E+01 |
| Surface # | 9 | 10 | 11 | 12 | 13 | 14 | 15 |
| k = | 4.46152E+01 | -1.21157E+01 | 3.14795E+01 | -2.47288E+01 | -1.16100E+01 | -5.59566E+00 | -5.00000E+01 |
| A4 = | -1.94943E-01 | -6.68441E-02 | -9.15225E-02 | -7.78137E-02 | -1.80510E-02 | -6.27769E-04 | -3.90311E-03 |
| A6 = | -1.41164E-02 | -1.80080E-02 | 2.24093E-02 | 7.31816E-03 | 6.90744E-04 | -3.48857E-04 | -7.35430E-04 |
| A8 = | 3.58467E-03 | -1.90471E-02 | -3.57962E-03 | 3.47773E-03 | -1.86583E-04 | 3.72209E-04 | 3.83260E-04 |
| A10 = | 2.91847E-02 | | | -9.16531E-04 | 6.83644E-06 | -3.16997E-05 | -1.17201E-05 |
| A12 = | | | | | | -1.14494E-07 | -1.12308E-06 |

In the optical image capturing lenses according to the second embodiment, the definitions of f, Fno, HFOV, FOV, CT1, CT2, f1, if, fr, CRmax, DIST, SAG11 and YD1 are the same as those stated in the first embodiment with corresponding values for the second embodiment. Rn1 and Rn2 are the curvature radius of the surfaces of the sixth lens element 260 which has negative refractive power and is nearest to the image plane 280. Moreover, these parameters can be calculated from Table 3 as the following values and satisfy the following relationships:

| 2nd Embodiment | | | |
|-------------------------|------|--------------|-------|
| f (mm) | 4.61 | f/f1 | -0.23 |
| Fno | 7.00 | fr/ff | -0.25 |
| HFOV (deg.) | 38.5 | CRmax (deg.) | 14.0 |
| FOV (deg.) | 77.0 | DIST [%] | -34.9 |
| CT1/CT2 | 2.57 | SAG11/YD1 | 0.66 |
| (Rn1 - Rn2)/(Rn1 + Rn2) | 0.38 | | |

FIG. 5 is a schematic view of an optical image capturing lenses according to the third embodiment of the present disclosure. FIG. 6 shows spherical aberration curves, astigmatic field curves and a distortion curve of the optical image capturing lenses according to the third embodiment. In FIG. 5, the optical image capturing lenses includes, in order from an object side to an image side, the first lens element 310, the

second lens element 320, the third lens element 330, an aperture stop 300, the fourth lens element 340, the fifth lens element 350, the sixth lens element 360, the seventh lens element 370, an IR cut filter 390, an image plane 380 and an image sensor 381. The first lens to element 310, the second lens element 320 and the third lens element 330 belong to a front lens group. The fourth lens element 340, the fifth lens element 350, the sixth lens element 360 and the seventh lens element 370 belong to a rear lens group.

The first lens element 310 with negative refractive power has a convex object-side surface 311 and a concave image-side surface 312, and is made of plastic material. The object-side surface 311 and the image-side surface 312 of the first lens element 310 are aspheric.

The second lens element 320 with negative refractive power has a convex object-side surface 321 and a concave image-side surface 322, and is made of plastic material. The object-side surface 321 and the image-side surface 322 of the second lens element 320 are aspheric.

The third lens element 330 with positive refractive power has a concave object-side surface 331 and a convex image-side surface 332, and is made of plastic material. The object-side surface 331 and the image-side surface 332 of the third lens element 330 are aspheric.

The fourth lens element 340 with negative refractive power has a concave object-side surface 341 and a concave image-side surface 342, and is made of plastic material. The object-

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side surface **341** and the image-side surface **342** of the fourth lens element **340** are aspheric.

The fifth lens element **350** with positive refractive power has a convex object-side surface **351** and a convex image-side surface **352**, and is made of plastic material. The object-side surface **351** and the image-side surface **352** of the fifth lens element **350** are aspheric. Moreover, the fifth lens element **350** has inflection points formed on the object-side surface **351** thereof.

The sixth lens element **360** with negative refractive power has a convex object-side surface **361** and a concave image-side surface **362**, and is made of plastic material. The object-side surface **361** and the image-side surface **362** of the sixth lens element **360** are aspheric. Moreover, the sixth lens element **360** has inflection points formed on the object-side surface **361** and the image-side surface **362** thereof.

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The seventh lens element **370** with positive refractive power has a convex object-side surface **371** and a concave image-side surface **372**, and is made of plastic material. The object-side surface **371** and the image-side surface **372** of the seventh lens element **370** are aspheric. Moreover, the seventh lens element **370** has inflection points formed on the object-side surface **371** and the image-side surface **372** thereof.

The IR cut filter **390** is made of glass and located between the seventh lens element **370** and the image plane **380**, and will not affect the focal length of the optical image capturing lenses.

The detailed optical data of the third embodiment are shown in Table 5 and the aspheric surface data are shown in Table 6 below.

TABLE 5

| 3rd Embodiment | | | | | | | |
|---|-----------|------------------|-----------|----------|-------|--------|--------------|
| f = 4.62 mm, Fno = 7.00, HFOV = 38.5 deg. | | | | | | | |
| Surface # | | Curvature Radius | Thickness | Material | Index | Abbe # | Focal length |
| 0 | Object | Plano | Infinity | | | | |
| 1 | Lens 1 | 2.959416 (ASP) | 1.969 | Plastic | 1.535 | 56.3 | -21.92 |
| 2 | | 1.815106 (ASP) | 1.516 | | | | |
| 3 | Lens 2 | 4.662425 (ASP) | 0.700 | Plastic | 1.650 | 21.4 | -29.74 |
| 4 | | 3.534092 (ASP) | 0.796 | | | | |
| 5 | Lens 3 | -21.265512 (ASP) | 1.011 | Plastic | 1.535 | 56.3 | 12.61 |
| 6 | | -5.204419 (ASP) | 0.086 | | | | |
| 7 | Ape. Stop | Plano | 0.114 | | | | |
| 8 | Lens 4 | -16.236668(ASP) | 0.700 | Plastic | 1.544 | 55.9 | -7.41 |
| 9 | | 5.443969 (ASP) | 0.246 | | | | |
| 10 | Lens 5 | 2.318196 (ASP) | 1.180 | Plastic | 1.544 | 55.9 | 3.50 |
| 11 | | -8.752174 (ASP) | 0.150 | | | | |
| 12 | Lens 6 | 2.878664 (ASP) | 0.600 | Plastic | 1.650 | 21.4 | -4.22 |
| 13 | | 1.288461 (ASP) | 0.953 | | | | |
| 14 | Lens 7 | 1.019347 (ASP) | 1.479 | Plastic | 1.544 | 55.9 | 3.11 |
| 15 | | 1.253942 (ASP) | 0.550 | | | | |
| 16 | IR-filter | Plano | 0.400 | Glass | 1.517 | 64.2 | — |
| 17 | | Plano | 0.899 | | | | |
| 18 | Image | Plano | — | | | | |

Note:

Reference wavelength (d-line) is 587.6 nm.

TABLE 6

| Aspheric Coefficient | | | | | | | |
|----------------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|
| Surface # | 1 | 2 | 3 | 4 | 5 | 6 | 8 |
| k = | -6.66904E-01 | -8.06674E-01 | -5.23609E+00 | -1.92745E+01 | 4.99999E+01 | 3.52522E+00 | 5.00018E+01 |
| A4 = | 8.49057E-03 | 1.09523E-01 | 2.46714E-03 | -1.31458E-02 | -1.00515E-01 | -2.66654E-01 | -2.59507E-01 |
| A6 = | 1.55642E-03 | -2.88681E-02 | -3.03980E-04 | 6.88093E-03 | 5.71899E-02 | 2.76361E-01 | -2.85163E+00 |
| A8 = | -3.97804E-04 | 2.14788E-03 | 2.49245E-04 | 7.60282E-04 | 2.76976E-02 | -1.17633E+00 | 2.16117E+01 |
| A10 = | 1.86872E-05 | -2.92377E-05 | | | -8.92788E-02 | 8.57404E-01 | -5.67360E+01 |
| Surface # | 9 | 10 | 11 | 12 | 13 | 14 | 15 |
| k = | 5.13390E+00 | -8.10958E+00 | 3.63378E+01 | -5.00000E+01 | -1.78511E+01 | -4.86405E+00 | -5.00000E+01 |
| A4 = | -3.23313E-01 | -6.85279E-02 | -6.44253E-02 | -8.26997E-02 | -3.97196E-02 | -3.47272E-03 | -2.83377E-02 |
| A6 = | -9.53353E-02 | -3.20876E-02 | 1.84405E-02 | -3.83203E-03 | 1.81845E-03 | -1.83918E-03 | 2.74542E-03 |
| A8 = | 1.20016E-01 | -3.92679E-02 | -1.18612E-02 | 1.42459E-03 | 1.39100E-04 | 4.41056E-04 | 1.44976E-04 |
| A10 = | -3.26864E-02 | | | -7.43108E-04 | -5.29977E-05 | -7.24289E-06 | -3.23522E-05 |
| A12 = | | | | | | -3.40028E-06 | 3.02160E-07 |

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In the optical image capturing lenses according to the third embodiment, the definitions of f , Fno , $HFOV$, FOV , $CT1$, $CT2$, $f1$, f , fr , CRA_{max} , $DIST$, $SAG11$ and $YD1$ are the same as those stated in the first embodiment with corresponding values for the third embodiment. $Rn1$ and $Rn2$ are the curvature radius of the surfaces of the sixth lens element **360** which has negative refractive power and is nearest to the image plane **380**. Moreover, these parameters can be calculated from Table 5 as the following values and satisfy the following relationships:

| 3rd Embodiment | | | |
|---------------------------|------|--------------------|-------|
| f (mm) | 4.62 | $f/1$ | -0.21 |
| Fno | 7.00 | $fr/1$ | -0.01 |
| $HFOV$ (deg.) | 38.5 | CRA_{max} (deg.) | 4.6 |
| FOV (deg.) | 77.0 | $DIST$ [%] | -35.0 |
| $CT1/CT2$ | 2.81 | $SAG11/YD1$ | 0.68 |
| $(Rn1 - Rn2)/(Rn1 + Rn2)$ | 0.38 | | |

FIG. 7 is a schematic view of an optical image capturing lenses according to the fourth embodiment of the present disclosure. FIG. 8 shows spherical aberration curves, astigmatic field curves and a distortion curve of the optical image capturing lenses according to the fourth embodiment. In FIG. 7, the optical image capturing lenses includes, in order from an object side to an image side, the first lens element **410**, the second lens element **420**, the third lens element **430**, an aperture stop **400**, the fourth lens element **440**, the fifth lens element **450**, the sixth lens element **460**, the seventh lens element **470**, an IR cut filter **490**, an image plane **480** and an image sensor **481**. The first lens element **410**, the second lens element **420** and the third lens element **430** belong to a front lens group. The fourth lens element **440**, the fifth lens element **450**, the sixth lens element **460** and the seventh lens element **470** belong to a rear lens group.

The first lens element **410** with negative refractive power has a convex object-side surface **411** and a concave image-side surface **412**, and is made of plastic material. The object-side surface **411** and the image-side surface **412** of the first lens element **410** are aspheric.

The second lens element **420** with negative refractive power has a convex object-side surface **421** and a concave

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image-side surface **422**, and is made of plastic material. The object-side surface **421** and the image-side surface **422** of the second lens element **420** are aspheric.

The third lens element **430** with positive refractive power has a convex object-side surface **431** and a convex image-side surface **432**, and is made of plastic material. The object-side surface **431** and the image-side surface **432** of the third lens element **430** are aspheric.

The fourth lens element **440** with negative refractive power has a convex object-side surface **441** and a concave image-side surface **442**, and is made of plastic material. The object-side surface **441** and the image-side surface **442** of the fourth lens element **440** are aspheric.

The fifth lens element **450** with positive refractive power has a convex object-side surface **451** and a convex image-side surface **452**, and is made of plastic material. The object-side surface **451** and the image-side surface **452** of the fifth lens element **450** are aspheric. Moreover, the fifth lens element **450** has inflection points formed on the object-side surface **451** thereof.

The sixth lens element **460** with negative refractive power has a convex object-side surface **461** and a concave image-side surface **462**, and is made of plastic material. The object-side surface **461** and the image-side surface **462** of the sixth lens element **460** are aspheric. Moreover, the sixth lens element **460** has inflection points formed on the object-side surface **461** and the image-side surface **462** thereof.

The seventh lens element **470** with positive refractive power has a convex object-side surface **471** and a concave image-side surface **472**, and is made of plastic material. The object-side surface **471** and the image-side surface **472** of the seventh lens element **470** are aspheric. Moreover, the seventh lens element **470** has inflection points formed on the object-side surface **471** and the image-side surface **472** thereof.

The IR cut filter **490** is made of glass and located between the seventh lens element **470** and the image plane **480**, and will not affect the focal length of the optical image capturing lenses.

The detailed optical data of the fourth embodiment are shown in Table 7 and the aspheric surface data are shown in Table 8 below.

TABLE 7

| 4th Embodiment | | | | | | | |
|--|-----------|------------------|-----------|----------|-------|--------|--------------|
| $f = 4.61$ mm, $Fno = 7.00$, $HFOV = 38.5$ deg. | | | | | | | |
| Surface # | | Curvature Radius | Thickness | Material | Index | Abbe # | Focal length |
| 0 | Object | Plano | Infinity | | | | |
| 1 | Lens 1 | 3.114400 (ASP) | 2.062 | Plastic | 1.535 | 56.3 | -29.75 |
| 2 | | 2.003610 (ASP) | 1.387 | | | | |
| 3 | Lens 2 | 3.447928 (ASP) | 0.700 | Plastic | 1.650 | 21.4 | -18.72 |
| 4 | | 2.471691 (ASP) | 0.828 | | | | |
| 5 | Lens 3 | 15.888210 (ASP) | 1.027 | Plastic | 1.535 | 56.3 | 9.90 |
| 6 | | -7.757020 (ASP) | 0.113 | | | | |
| 7 | Ape. Stop | Plano | 0.106 | | | | |
| 8 | Lens 4 | 30.183699 (ASP) | 0.751 | Plastic | 1.544 | 55.9 | -7.80 |
| 9 | | 3.686878 (ASP) | 0.220 | | | | |
| 10 | Lens 5 | 2.383992 (ASP) | 1.191 | Plastic | 1.544 | 55.9 | 3.59 |
| 11 | | -8.966837 (ASP) | 0.150 | | | | |
| 12 | Lens 6 | 8.697503 (ASP) | 0.600 | Plastic | 1.650 | 21.4 | -3.97 |
| 13 | | 1.934436 (ASP) | 0.878 | | | | |
| 14 | Lens 7 | 1.032642 (ASP) | 1.487 | Plastic | 1.544 | 55.9 | 2.81 |
| 15 | | 1.566092 (ASP) | 0.550 | | | | |
| 16 | IR-filter | Plano | 0.400 | Glass | 1.517 | 64.2 | — |

TABLE 7-continued

| 4th Embodiment f = 4.61 mm, Fno = 7.00, HFOV = 38.5 deg. | | | | | | |
|---|------------------|-----------|----------|-------|--------|--------------|
| Surface # | Curvature Radius | Thickness | Material | Index | Abbe # | Focal length |
| 17 | Plano | 0.891 | | | | |
| 18 Image | Plano | — | | | | |

Note:
Reference wavelength (d-line) is 587.6 nm.

TABLE 8

| Aspheric Coefficients | | | | | | | |
|-----------------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|
| Surface # | 1 | 2 | 3 | 4 | 5 | 6 | 8 |
| k = | -7.90085E-01 | -3.90841E-01 | -5.24394E+00 | -2.00000E+01 | -5.00000E+01 | 1.75058E+01 | 5.00000E+01 |
| A4 = | 9.97460E-03 | 1.23594E-01 | 4.83278E-03 | -1.42084E-02 | -1.01915E-01 | -2.82760E-01 | -2.20498E-01 |
| A6 = | 1.45115E-03 | -2.68205E-02 | 2.90062E-05 | 7.11017E-03 | 5.68640E-02 | 4.00305E-01 | -2.87048E+00 |
| A8 = | -3.95396E-04 | 2.11932E-03 | 3.19915E-04 | 1.20479E-03 | 2.93392E-02 | -2.00840E+00 | 2.30204E+01 |
| A10 = | 1.91805E-05 | -9.92264E-05 | | | -8.88621E-02 | 3.45595E+00 | -6.25899E+01 |
| Surface # | 9 | 10 | 11 | 12 | 13 | 14 | 15 |
| k = | 1.05690E+01 | -9.02403E+00 | 3.65937E+01 | -4.00132E+01 | -3.11504E+01 | -4.38686E+00 | -4.91761E+01 |
| A4 = | -3.19178E-01 | -6.39240E-02 | -5.73492E-02 | -8.73835E-02 | -4.29192E-02 | -5.40488E-04 | -2.33126E-02 |
| A6 = | -9.95448E-02 | -3.73047E-02 | 1.84512E-02 | -3.05189E-03 | 1.45610E-03 | -2.04179E-03 | 2.74200E-03 |
| A8 = | 1.54264E-01 | -4.14431E-02 | -1.16057E-02 | 1.71439E-03 | 1.73462E-04 | 4.39949E-04 | 1.08498E-04 |
| A10 = | -9.90086E-02 | | | -5.11708E-04 | -2.07175E-05 | -3.72317E-06 | -3.43193E-05 |
| A12 = | | | | | | -3.54629E-06 | 7.68676E-07 |

In the optical image capturing lenses according to the fourth embodiment, the definitions of f, Fno, HFOV, FOV, CT1, CT2, f1, f, fr, CRAMax, DIST, SAG11 and YD1 are the same as those stated in the first embodiment with corresponding values for the fourth embodiment. Rn1 and Rn2 are the curvature radius of the surfaces of the sixth lens element 460 which has negative refractive power and is nearest to the image plane 480. Moreover, these parameters can be calculated from Table 7 as the following values and satisfy the following relationships:

| 4th Embodiment | | | |
|-------------------------|------|---------------|-------|
| f (mm) | 4.61 | f/fl | -0.16 |
| Fno | 7.00 | fr/ff | 0.03 |
| HFOV (deg.) | 38.5 | CRAMax (deg.) | 4.4 |
| FOV (deg.) | 77.0 | DIST [%] | -34.9 |
| CT1/CT2 | 2.95 | SAG11/YD1 | 0.65 |
| (Rn1 - Rn2)/(Rn1 + Rn2) | 0.64 | | |

FIG. 9 is a schematic view of an optical image capturing lenses according to the fifth embodiment of the present disclosure. FIG. 10 shows spherical to aberration curves, astigmatic field curves and a distortion curve of the optical image capturing lenses according to the fifth embodiment. In FIG. 9, the optical image capturing lenses includes, in order from an object side to an image side, the first lens element 510, the second lens element 520, the third lens element 530, an aperture stop 500, the fourth lens element 540, the fifth lens element 550, the sixth lens element 560, the seventh lens element 570, an IR cut filter 590, an image plane 580 and an image sensor 581. The first lens element 510, the second lens element 520 and the third lens element 530 belong to a front lens group. The fourth lens element 540, the fifth lens element

550, the sixth lens element 560 and the seventh lens element 570 belong to a rear lens group.

The first lens element 510 with positive refractive power has a convex object-side surface 511 and a concave image-side surface 512, and is made of plastic material. The object-side surface 511 and the image-side surface 512 of the first lens element 510 are aspheric.

The second lens element 520 with negative refractive power has a convex object-side surface 521 and a concave image-side surface 522, and is made of plastic material. The object-side surface 521 and the image-side surface 522 of the second lens element 520 are aspheric.

The third lens element 530 with negative refractive power has a concave to object-side surface 531 and a convex image-side surface 532, and is made of plastic material. The object-side surface 531 and the image-side surface 532 of the third lens element 530 are aspheric.

The fourth lens element 540 with negative refractive power has a convex object-side surface 541 and a concave image-side surface 542, and is made of plastic material. The object-side surface 541 and the image-side surface 542 of the fourth lens element 540 are aspheric.

The fifth lens element 550 with positive refractive power has a convex object-side surface 551 and a convex image-side surface 552, and is made of plastic material. The object-side surface 551 and the image-side surface 552 of the fifth lens element 550 are aspheric. Moreover, the fifth lens element 550 has inflection points formed on the object-side surface 551 thereof.

The sixth lens element 560 with negative refractive power has a convex object-side surface 561 and a concave image-side surface 562, and is made of plastic material. The object-side surface 561 and the image-side surface 562 of the sixth lens element 560 are aspheric. Moreover, the sixth lens ele-

ment **560** has inflection points formed on the object-side surface **561** and the image-side surface **562** thereof.

The seventh lens element **570** with positive refractive power has a convex object-side surface **571** and a concave image-side surface **572**, and is made of plastic material. The object-side surface **571** and the image-side surface **572** of the seventh lens element **570** are aspheric. Moreover, the seventh lens element **570** has inflection points formed on the object-side surface **571** and the image-side surface **572** thereof.

The IR cut filter **590** is made of glass and located between the seventh lens element **570** and the image plane **580**, and will not affect the focal length of the optical image capturing lenses.

The detailed optical data of the fifth embodiment are shown in Table 9 and the aspheric surface data are shown in Table 10 below.

TABLE 9

| 5th Embodiment | | | | | | | |
|---|-----------|------------------|-----------|----------|-------|--------|--------------|
| f = 4.61 mm, Fno = 7.00, HFOV = 38.5 deg. | | | | | | | |
| Surface # | | Curvature Radius | Thickness | Material | Index | Abbe # | Focal length |
| 0 | Object | Plano | Infinity | | | | |
| 1 | Lens 1 | 2.558346 (ASP) | 2.046 | Plastic | 1.535 | 56.3 | 54.85 |
| 2 | | 2.022127 (ASP) | 0.866 | | | | |
| 3 | Lens 2 | 4.656237 (ASP) | 0.700 | Plastic | 1.614 | 25.6 | -6.79 |
| 4 | | 2.073778 (ASP) | 0.678 | | | | |
| 5 | Lens 3 | -7.922119 (ASP) | 1.557 | Plastic | 1.535 | 56.3 | 39.52 |
| 6 | | -6.156170 (ASP) | 0.111 | | | | |
| 7 | Ape. Stop | Plano | 0.089 | | | | |
| 8 | Lens 4 | 4.241957 (ASP) | 0.981 | Plastic | 1.544 | 55.9 | -39.27 |
| 9 | | 3.250798 (ASP) | 0.254 | | | | |
| 10 | Lens 5 | 2.185827 (ASP) | 1.225 | Plastic | 1.544 | 55.9 | 3.34 |
| 11 | | -8.675449 (ASP) | 0.150 | | | | |
| 12 | Lens 6 | 13.180914 (ASP) | 0.679 | Plastic | 1.614 | 25.6 | -2.90 |
| 13 | | 1.536786 (ASP) | 0.527 | | | | |
| 14 | Lens 7 | 0.949471 (ASP) | 1.293 | Plastic | 1.544 | 55.9 | 2.38 |
| 15 | | 1.843935 (ASP) | 0.557 | | | | |
| 16 | IR-filter | Plano | 0.400 | Glass | 1.517 | 64.2 | — |
| 17 | | Plano | 0.894 | | | | |
| 18 | Image | Plano | — | | | | |

Note:

Reference wavelength (d-line) is 587.6 nm.

ture radius of the surfaces of the sixth lens element **560** which has negative refractive power and is nearest to the image plane **580**. Moreover, these parameters can be calculated from Table 9 as the following values and satisfy the following relationships:

| 5th Embodiment | | | |
|-------------------------|------|---------------|-------|
| f (mm) | 4.61 | f/fl | 0.08 |
| Fno | 7.00 | fr/ff | -0.19 |
| HFOV (deg.) | 38.5 | CRAMax (deg.) | 10.0 |
| FOV (deg.) | 77.0 | DIST [%] | -34.9 |
| CT1/CT2 | 2.92 | SAG11/YD1 | 0.58 |
| (Rn1 - Rn2)/(Rn1 + Rn2) | 0.79 | | |

TABLE 10

| Aspheric Coefficients | | | | | | | |
|-----------------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|
| Surface # | 1 | 2 | 3 | 4 | 5 | 6 | 8 |
| k = | -1.15755E+00 | -3.82916E-01 | -1.85403E+00 | -1.50199E+01 | 3.55540E+01 | 2.00000E+01 | 6.33300E+00 |
| A4 = | 6.50322E-03 | 6.72099E-02 | -2.19758E-04 | -2.31974E-02 | -1.31992E-01 | -2.36455E-01 | -2.30529E-01 |
| A6 = | 1.22218E-03 | -2.83902E-02 | 9.78060E-05 | 2.55145E-03 | 8.05976E-02 | 4.14719E-01 | -2.66520E+00 |
| A8 = | -3.87204E-04 | 2.16689E-03 | 1.76835E-04 | 1.98541E-03 | -1.03851E-02 | -4.77934E-01 | 3.17896E+01 |
| A10 = | 2.01527E-05 | 3.61587E-06 | | | -1.79989E-03 | 2.92045E-01 | -1.20124E+02 |
| Surface # | 9 | 10 | 11 | 12 | 13 | 14 | 15 |
| k = | 1.06812E+01 | -7.53314E+00 | 3.94629E+01 | -4.47825E+00 | -2.48475E+01 | -5.40697E+00 | -5.00000E+01 |
| A4 = | -3.02669E-01 | -3.55566E-02 | -8.23500E-02 | -1.32388E-01 | -5.07720E-02 | -1.32573E-02 | -1.69160E-02 |
| A6 = | -7.47478E-02 | -2.83389E-02 | 2.38892E-02 | -2.18380E-02 | 7.77131E-04 | -1.04154E-03 | 5.97355E-04 |
| A8 = | 1.73000E-01 | -1.32474E-02 | -1.11130E-02 | 5.10373E-03 | 4.39629E-04 | 4.52290E-04 | 1.17868E-04 |
| A10 = | -2.11402E-01 | | | -1.55294E-03 | 1.84802E-04 | 5.24114E-06 | -2.83144E-05 |
| A12 = | | | | | | -4.48681E-06 | 1.73524E-06 |

In the optical image capturing lenses according to the fifth embodiment, the definitions of f, Fno, HFOV, FOV, CT1, CT2, fl, f, fr, CRAMax, DIST, SAG11 and YD1 are the same as those stated in the first embodiment with corresponding values for the fifth embodiment. Rn1 and Rn2 are the curva-

FIG. 11 is a schematic view of an optical image capturing lenses according to the sixth embodiment of the present disclosure. FIG. 12 shows spherical aberration curves, astigmatic field curves and a distortion curve of the optical image capturing lenses according to the sixth embodiment. In FIG.

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11, the optical image capturing lenses includes, in order from an object side to an image side, the first lens element 610, the second lens element 620, the third lens element 630, an aperture stop 600, the fourth lens element 640, the fifth lens element 650, the sixth lens element 660, the seventh lens element 670, an IR cut filter 690, an image plane 680 and an image sensor 681. The first lens element 610, the second lens element 620 and the third lens element 630 belong to a front lens group. The fourth lens element 640, the fifth lens element 650, the sixth lens element 660 and the seventh lens element 670 belong to a rear lens group.

The first lens element 610 with positive refractive power has a convex object-side surface 611 and a concave image-side surface 612, and is made of plastic material. The object-side surface 611 and the image-side surface 612 of the first lens element 610 are aspheric.

The second lens element 620 with negative refractive power has a convex object-side surface 621 and a concave image-side surface 622, and is made of plastic material. The object-side surface 621 and the image-side surface 622 of the second lens element 620 are aspheric.

The third lens element 630 with negative refractive power has a concave object-side surface 631 and a concave image-side surface 632, and is made of plastic material. The object-side surface 631 and the image-side surface 632 of the third lens element 630 are aspheric.

The fourth lens element 640 with positive refractive power has a convex object-side surface 641 and a concave image-side surface 642, and is made of plastic material. The object-

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side surface 641 and the image-side surface 642 to of the fourth lens element 640 are aspheric.

The fifth lens element 650 with positive refractive power has a convex object-side surface 651 and a convex image-side surface 652, and is made of plastic material. The object-side surface 651 and the image-side surface 652 of the fifth lens element 650 are aspheric. Moreover, the fifth lens element 650 has inflection points formed on the object-side surface 651 thereof.

The sixth lens element 660 with negative refractive power has a concave object-side surface 661 and a concave image-side surface 662, and is made of plastic material. The object-side surface 661 and the image-side surface 662 of the sixth lens element 660 are aspheric. Moreover, the sixth lens element 660 has inflection points formed on the object-side surface 661 and the image-side surface 662 thereof.

The seventh lens element 670 with positive refractive power has a convex object-side surface 671 and a concave image-side surface 672, and is made of plastic material. The object-side surface 671 and the image-side surface 672 of the seventh lens element 670 are aspheric. Moreover, the seventh lens element 670 has inflection points formed on the object-side surface 671 and the image-side surface 672 thereof.

The IR cut filter 690 is made of glass and located between the seventh lens element 670 and the image plane 680, and will not affect the focal length of the optical image capturing lenses.

The detailed optical data of the sixth embodiment are shown in Table 11 and the aspheric surface data are shown in Table 12 below.

TABLE 11

| 6th Embodiment | | | | | | | |
|---|-----------|------------------|-----------|----------|-------|--------|--------------|
| f = 4.61 mm, Fno = 7.00, HFOV = 38.5 deg. | | | | | | | |
| Surface # | | Curvature Radius | Thickness | Material | Index | Abbe # | Focal length |
| 0 | Object | Plano | Infinity | | | | |
| 1 | Lens 1 | 2.564968 (ASP) | 1.987 | Plastic | 1.530 | 55.8 | 54.86 |
| 2 | | 2.058261 (ASP) | 0.811 | | | | |
| 3 | Lens 2 | 3.886640 (ASP) | 0.700 | Plastic | 1.614 | 25.6 | -6.55 |
| 4 | | 1.840862 (ASP) | 0.710 | | | | |
| 5 | Lens 3 | -7.650501 (ASP) | 1.615 | Plastic | 1.535 | 56.3 | -11.91 |
| 6 | | 40.765846 (ASP) | 0.117 | | | | |
| 7 | Ape. Stop | Plano | 0.083 | | | | |
| 8 | Lens 4 | 2.275256 (ASP) | 1.034 | Plastic | 1.544 | 55.9 | 10.23 |
| 9 | | 3.232066 (ASP) | 0.273 | | | | |
| 10 | Lens 5 | 2.120035 (ASP) | 1.650 | Plastic | 1.544 | 55.9 | 3.25 |
| 11 | | -7.778525 (ASP) | 0.150 | | | | |
| 12 | Lens 6 | -43.662185 (ASP) | 0.690 | Plastic | 1.614 | 25.6 | -2.74 |
| 13 | | 1.761903 (ASP) | 0.452 | | | | |
| 14 | Lens 7 | 0.990872 (ASP) | 1.280 | Plastic | 1.544 | 55.9 | 2.50 |
| 15 | | 1.991869 (ASP) | 0.450 | | | | |
| 16 | IR-filter | Plano | 0.400 | Glass | 1.517 | 64.2 | — |
| 17 | | Plano | 0.894 | | | | |
| 18 | Image | Plano | — | | | | |

Note:

Reference wavelength (d-line) is 587.6 nm.

TABLE 12

| Aspheric Coefficients | | | | | | | |
|-----------------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|
| Surface # | 1 | 2 | 3 | 4 | 5 | 6 | 8 |
| k = | -1.26767E+00 | -3.80803E-01 | -3.46093E+00 | -1.11629E+01 | 2.48768E+01 | 2.00000E+01 | 2.04228E+00 |
| A4 = | 6.16446E-03 | 6.67749E-02 | -1.78186E-03 | -2.30203E-02 | -1.28054E-01 | -3.02979E-01 | -2.51831E-01 |
| A6 = | 1.24005E-03 | -2.83454E-02 | 1.53412E-04 | 1.21697E-03 | 7.86739E-02 | 5.90778E-01 | -2.60579E+00 |
| A8 = | -3.85683E-04 | 2.19225E-03 | 2.23530E-04 | 2.13376E-03 | -1.61971E-02 | -1.92975E+00 | 3.00313E+01 |
| A10 = | 2.02990E-05 | 9.02400E-06 | | | 1.29120E-03 | 6.63586E+00 | -1.09487E+02 |

TABLE 12-continued

| Aspheric Coefficients | | | | | | | |
|-----------------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|
| Surface # | 9 | 10 | 11 | 12 | 13 | 14 | 15 |
| k = | 9.54250E+00 | -7.76544E+00 | 2.11469E+01 | 3.19251E+01 | -2.43762E+01 | -4.71919E+00 | -5.00000E+01 |
| A4 = | -2.93807E-01 | -3.97789E-02 | -1.07520E-01 | -1.20983E-01 | -5.37849E-02 | -1.48864E-02 | -1.22842E-02 |
| A6 = | -2.69030E-02 | -2.53026E-02 | 3.05348E-02 | -3.38065E-02 | 6.06328E-04 | -8.20607E-04 | 2.89124E-04 |
| A8 = | 1.59728E-01 | -1.11466E-03 | -9.79234E-03 | 6.13896E-03 | 4.27572E-04 | 4.54235E-04 | 1.19916E-04 |
| A10 = | -2.27773E-01 | | | 9.59411E-04 | 2.44904E-04 | 6.43179E-06 | -2.47917E-05 |
| A12 = | | | | | | -4.12729E-06 | 1.62316E-06 |

In the optical image capturing lenses according to the sixth embodiment, the definitions of f, Fno, HFOV, FOV, CT1, CT2, f1, if, fr, CRAMax, DIST, SAG11 and YD1 are the same as those stated in the first embodiment with corresponding values for the sixth embodiment. Rn1 and Rn2 are the curvature radius of the surfaces of the sixth lens element 660 which has negative refractive power and is nearest to the image plane 680. Moreover, these parameters can be calculated from Table 11 as the following values and satisfy the following relationships:

| 6th Embodiment | | | |
|-------------------------|------|---------------|-------|
| f (mm) | 4.61 | f/fl | 0.08 |
| Fno | 7.00 | fr/ff | -0.42 |
| HFOV (deg.) | 38.5 | CRAMax (deg.) | 9.9 |
| FOV (deg.) | 77.0 | DIST [%] | -34.9 |
| CT1/CT2 | 2.84 | SAG11/YD1 | 0.56 |
| (Rn1 - Rn2)/(Rn1 + Rn2) | 1.09 | | |

FIG. 13 is a schematic view of an optical image capturing lenses according to the seventh embodiment of the present disclosure. FIG. 14 shows spherical aberration curves, astigmatic field curves and a distortion curve of the optical image capturing lenses according to the seventh embodiment. In FIG. 13, the optical image capturing lenses includes, in order from an object side to an image side, the first lens element 710, the second lens element 720, the third lens element 730, an aperture stop 700, the fourth lens element 740, the fifth lens element 750, the sixth lens element 760, the seventh lens element 770, an IR cut filter 790, an image plane 780 and an image sensor 781. The first lens element 710, the second lens element 720 and the third lens element 730 belong to a front lens group. The fourth lens element 740, the fifth lens element 750, the sixth lens element 760 and the seventh lens element 770 belong to a rear lens group.

The first lens element 710 with positive refractive power has a convex object-side surface 711 and a concave image-side surface 712, and is made of plastic material. The object-side surface 711 and the image-side surface 712 of the first lens element 710 are aspheric.

The second lens element 720 with negative refractive power has a convex object-side surface 721 and a concave

image-side surface 722, and is made of plastic material. The object-side surface 721 and the image-side surface 722 of the second lens element 720 are aspheric.

The third lens element 730 with positive refractive power has a concave object-side surface 731 and a convex image-side surface 732, and is made of plastic material. The object-side surface 731 and the image-side surface 732 of the third lens element 730 are aspheric.

The fourth lens element 740 with negative refractive power has a convex object-side surface 741 and a concave image-side surface 742, and is made of plastic material. The object-side surface 741 and the image-side surface 742 of the fourth lens element 740 are aspheric.

The fifth lens element 750 with positive refractive power has a convex object-side surface 751 and a convex image-side surface 752, and is made of plastic material. The object-side surface 751 and the image-side surface 752 of the fifth lens element 750 are aspheric. Moreover, the fifth lens element 750 has inflection points formed on the object-side surface 751 thereof.

The sixth lens element 760 with negative refractive power has a concave object-side surface 761 and a concave image-side surface 762, and is made of plastic material. The object-side surface 761 and the image-side surface 762 of the sixth lens element 760 are aspheric. Moreover, the sixth lens element 760 has inflection points formed on the image-side surface 762 thereof.

The seventh lens element 770 with positive refractive power has a convex object-side surface 771 and a concave image-side surface 772, and is made of plastic material. The object-side surface 771 and the image-side surface 772 of the seventh lens element 770 are aspheric. Moreover, the seventh lens element 770 has inflection points formed on the object-side surface 771 and the image-side surface 772 thereof.

The IR cut filter 790 is made of glass and located between the seventh lens element 770 and the image plane 780, and will not affect the focal length of the optical image capturing lenses.

The detailed optical data of the seventh embodiment are shown in Table 13 and the aspheric surface data are shown in Table 14 below.

TABLE 13

| 7th Embodiment f = 4.61 mm, Fno = 7.00, HFOV = 38.5 deg. | | | | | | | |
|---|--------|------------------|-----------|----------|-------|--------|--------------|
| Surface # | | Curvature Radius | Thickness | Material | Index | Abbe # | Focal length |
| 0 | Object | Plano | Infinity | | | | |
| 1 | Lens 1 | 2.607357 (ASP) | 1.982 | Plastic | 1.530 | 55.8 | 56.30 |
| 2 | | 2.104843 (ASP) | 0.786 | | | | |

TABLE 13-continued

| 7th Embodiment f = 4.61 mm, Fno = 7.00, HFOV = 38.5 deg. | | | | | | | |
|---|-----------|------------------|-----------|----------|-------|--------|--------------|
| Surface # | | Curvature Radius | Thickness | Material | Index | Abbe # | Focal length |
| 3 | Lens 2 | 3.071470 (ASP) | 0.736 | Plastic | 1.614 | 25.6 | -6.72 |
| 4 | | 1.600401 (ASP) | 0.813 | | | | |
| 5 | Lens 3 | -7.966329 (ASP) | 1.735 | Plastic | 1.530 | 55.8 | 9.92 |
| 6 | | -3.405581 (ASP) | 0.102 | | | | |
| 7 | Ape. Stop | Plano | 0.098 | | | | |
| 8 | Lens 4 | 8.706769 (ASP) | 1.035 | Plastic | 1.544 | 55.9 | -10.95 |
| 9 | | 3.389086 (ASP) | 0.330 | | | | |
| 10 | Lens 5 | 2.287129 (ASP) | 1.464 | Plastic | 1.544 | 55.9 | 2.95 |
| 11 | | -4.181045 (ASP) | 0.150 | | | | |
| 12 | Lens 6 | -19.422994 (ASP) | 0.810 | Plastic | 1.614 | 25.6 | -2.57 |
| 13 | | 1.747843 (ASP) | 0.354 | | | | |
| 14 | Lens 7 | 0.934868 (ASP) | 1.101 | Plastic | 1.544 | 55.9 | 2.63 |
| 15 | | 1.581869 (ASP) | 0.450 | | | | |
| 16 | IR-filter | Plano | 0.400 | Glass | 1.517 | 64.2 | — |
| 17 | | Plano | 0.894 | | | | |
| 18 | Image | Plano | — | | | | |

Note:

Reference wavelength (d-line) is 587.6 nm.

TABLE 14

| Aspheric Coefficients | | | | | | | |
|-----------------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|
| Surface # | 1 | 2 | 3 | 4 | 5 | 6 | 8 |
| k = | -1.21043E+00 | -3.69303E-01 | -5.20080E+00 | -7.91577E+00 | 7.60001E+00 | -6.27221E+00 | -4.60529E+01 |
| A4 = | 6.29535E-03 | 6.73096E-02 | -4.28562E-03 | -2.47002E-02 | -1.19981E-01 | -2.86077E-01 | -2.58597E-01 |
| A6 = | 1.27726E-03 | -2.80677E-02 | 2.85291E-04 | 8.35532E-05 | 7.57241E-02 | 7.85768E-01 | -2.42393E+00 |
| A8 = | -3.85460E-04 | 2.23174E-03 | 3.44922E-04 | 4.16647E-03 | -2.17726E-02 | -3.62683E+00 | 2.86448E+01 |
| A10 = | 2.02332E-05 | 1.05448E-05 | | | 1.87395E-03 | 9.82829E+00 | -1.04677E+02 |
| Surface # | 9 | 10 | 11 | 12 | 13 | 14 | 15 |
| k = | 1.10848E+01 | -5.24838E+00 | 2.33963E+00 | -3.91464E+01 | -4.47593E+01 | -7.59124E+00 | -5.00000E+01 |
| A4 = | -3.04606E-01 | -4.22504E-02 | -1.30036E-01 | -1.32843E-01 | -3.46151E-02 | -2.87453E-02 | -2.37772E-02 |
| A6 = | -2.14266E-02 | -1.84018E-02 | 3.63886E-02 | -3.07364E-02 | -9.94951E-04 | -2.81416E-04 | -2.96345E-04 |
| A8 = | 1.25362E-01 | -9.58642E-04 | -5.59093E-03 | 1.27513E-02 | 2.88027E-04 | 4.43962E-04 | 2.41184E-04 |
| A10 = | -1.36523E-01 | | | 2.43520E-03 | 2.58535E-04 | 8.40337E-06 | -2.56288E-05 |
| A12 = | | | | | | -6.44926E-06 | -1.99547E-06 |

In the optical image capturing lenses according to the seventh embodiment, the definitions of f, Fno, HFOV, FOV, CT1, CT2, f1, if, fr, CRmax, DIST, SAG11 and YD1 are the same as those stated in the first embodiment with corresponding values for the seventh embodiment. Rn1 and Rn2 are the curvature radius of the surfaces of the sixth lens element 760 which has negative refractive power and is nearest to the image plane 780. Moreover, these parameters can be calculated from Table 13 as the following values and satisfy the following relationships:

| 7th Embodiment | | | |
|-------------------------|------|--------------|-------|
| f (mm) | 4.61 | f/f1 | 0.08 |
| Fno | 7.00 | fr/ff | 0.005 |
| HFOV (deg.) | 38.5 | CRmax (deg.) | 11.2 |
| FOV (deg.) | 77.0 | DIST [%] | -34.9 |
| CT1/CT2 | 2.69 | SAG11/YD1 | 0.58 |
| (Rn1 - Rn2)/(Rn1 + Rn2) | 1.20 | | |

It will be apparent to those skilled in the art that various modifications and variations can be made to the structure of the present invention without departing from the scope or

spirit of the invention. In view of the foregoing, it is intended that the present invention cover modifications and variations of this invention provided they fall within the scope of the following claims.

What is claimed is:

1. An optical image capturing lenses comprising, in order from an object side to an image side:
 - a first lens element having an object-side surface being convex in a paraxial region thereof and an image-side surface being concave in a paraxial region thereof;
 - a second lens element with negative refractive power having an object-side surface being convex in a paraxial region thereof and an image-side surface being concave in a paraxial region thereof;
 - a third lens element;
 - a fourth lens element having positive refractive power;
 - a fifth lens element made of plastic material, wherein an object-side surface and an image-side surface of the fifth lens element are aspheric; and
 - a sixth lens element having an object-side surface being convex in a paraxial region thereof and an image-side surface being concave in a paraxial region thereof and made of plastic material, wherein the object-side surface

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and the image-side surface of the sixth lens element are aspheric, and the image-side surface of the sixth lens element has at least one inflection point thereon wherein the optical image capturing lenses has a total of six lens elements, there is an air gap in a paraxial region between any two of the first lens element, the second lens element, the third lens element, the fourth lens element, the fifth lens element and the sixth lens element that are adjacent to each other, the optical image capturing lenses further comprises an aperture stop which is located at a side of the third lens element facing the object side, and a central thickness of the first lens element is larger than a central thickness of the second lens element.

2. The optical image capturing lenses of claim 1, wherein the object-side surface of the sixth lens element has at least one inflection point thereon.

3. The optical image capturing lenses of claim 2, wherein the third lens element has an image-side surface being concave in a paraxial region thereof.

4. The optical image capturing of claim 2, wherein the fourth lens element has an object-side surface being convex in a paraxial region thereof.

5. The optical image capturing lenses of claim 2, wherein the fifth lens element has negative refractive power.

6. The optical image capturing lenses of claim 2, wherein at least one of the object-side surface and the image-side surface of the fifth lens element has at least one inflection point thereon.

7. The optical image capturing lenses of claim 2, wherein the image-side surface of the fifth lens element is concave in a paraxial region thereof.

8. The optical image capturing lenses of claim 2, wherein a curvature radius of an object-side surface of the lens element nearest to an image plane with negative refractive power is $Rn1$, a curvature radius of an image-side surface of the lens element nearest to the image plane with negative refractive power is $Rn2$, the following relationship is satisfied:

$$0 < (Rn1 - Rn2) / (Rn1 + Rn2) < 1.5.$$

9. The optical image capturing lenses of claim 2, wherein a maximal field of view of the optical image capturing lenses is FOV, the following relationship is satisfied:

$$55 \text{ degrees} < \text{FOV} < 90 \text{ degrees}.$$

10. The optical image capturing lenses of claim 2, wherein a modulus of a focal length of the fifth lens element and a modulus of a focal length of the sixth lens element are larger than a modulus of a focal length of the fourth lens element.

11. The optical image capturing lenses of claim 1, wherein the fourth lens element has an image-side surface being convex in a paraxial region thereof.

12. The optical image capturing lenses of claim 1, wherein at least one of an object-side surface and an image-side surface of the fourth lens element has at least one inflection point thereon.

13. The optical image capturing lenses of claim 1, wherein the third lens element has positive refractive power.

14. The optical image capturing lenses of claim 1, wherein the third lens element has an object-side surface being convex in a paraxial region thereof.

15. The optical image capturing lenses of claim 1, wherein the object-side surface of the fifth lens element is convex in a paraxial region thereof.

16. The optical image capturing lenses of claim 1, wherein the object-side surface and the image-side surface of each of

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the first lens element, the second lens element, the third lens element and the fourth lens element are aspheric.

17. The optical image capturing lenses of claim 1, wherein the central thickness of the first lens element is $CT1$, and the central thickness of the second lens element is $CT2$, the following relationship is satisfied:

$$2.0 < CT1/CT2 < 3.5.$$

18. The optical image capturing lenses of claim 1, wherein a maximum SAG of an effective aperture on the object-side surface of the first lens element is $SAG11$, and an effective radius of the object-side surface of the first lens element is $YD1$, the following relationship is satisfied:

$$0.3 < SAG11/YD1 < 1.0.$$

19. The optical image capturing lenses of claim 1, wherein an axial distance between the fourth lens element and the fifth lens element is smaller than an axial distance between the fifth lens element and the sixth lens element.

20. The optical image capturing lenses of claim 1, wherein five of the first lens element, the second lens element, the third lens element, the fourth lens element, the fifth lens element and the sixth lens element has an object-side surface being convex in a paraxial region thereof and an image-side surface being concave in a paraxial region thereof.

21. An optical image capturing lenses comprising, in order from an object side to an image side:

a first lens element having an object-side surface being convex in a paraxial region thereof;

a second lens element having an object-side surface being convex in a paraxial region thereof;

a third lens element,

a fourth lens element having positive refractive power;

a fifth lens element made of plastic material, wherein an object-side surface and an image-side surface of the fifth lens element are aspheric; and

a sixth lens element with positive refractive power having an object-side surface being convex in a paraxial region thereof and an image-side surface being concave in a paraxial region thereof and made of plastic material, wherein the object-side surface and the image-side surface of the sixth lens element are aspheric, and the image-side surface of the sixth lens element has at least one inflection point thereon;

wherein the optical image capturing lenses has a total of six lens elements, there is an air gap in a paraxial region between any two of the first lens element, the second lens element, the third lens element, the fourth lens element, the fifth lens element and the sixth lens element that are adjacent to each other, the optical image capturing lenses further comprises an aperture stop which is located at a side of the third lens element facing the object side.

22. The optical image capturing lenses of claim 21, wherein the object-side surface of the sixth lens element has at least one inflection point thereon.

23. The optical image capturing lenses of claim 22, wherein the first lens element has an image-side surface being concave in a paraxial region thereof.

24. The optical image capturing lenses of claim 22, wherein the second lens element has an image-side surface being concave in a paraxial region thereof.

25. The optical image capturing lenses of claim 22, wherein the object-side surface of the fifth lens element is convex in a paraxial region thereof.

26. The optical image capturing lenses of claim 22, wherein the first lens element has negative refractive power.

27. The optical image capturing lenses of claim 22, wherein the fifth lens element has negative refractive power.

28. The optical image capturing lenses of claim 22, wherein the fourth lens element has an image-side surface being convex in a paraxial region thereof. 5

29. The optical image capturing lenses of claim 22, wherein a maximal field of view of the optical image capturing lenses is FOV, the following relationship is satisfied:

$$55 \text{ degrees} < \text{FOV} < 90 \text{ degrees.}$$

30. The optical image capturing lenses of claim 22, wherein a focal length of the optical image capturing lenses is f , a focal length of the first lens element is f_1 , the following relationship is satisfied: 10

$$-0.6 < f/f_1 < 0.3.$$

31. The optical image capturing lenses of claim 22, wherein an axial distance between the second lens element and the third lens element is smaller than an axial thickness of the third lens element. 15

32. The optical image capturing lenses of claim 22, wherein at least one of the object-side surface and the image-side surface of the fifth lens element has at least one inflection point thereon. 20

* * * * *

UNITED STATES PATENT AND TRADEMARK OFFICE
CERTIFICATE OF CORRECTION

PATENT NO. : 9,335,513 B2
APPLICATION NO. : 14/300219
DATED : May 10, 2016
INVENTOR(S) : Hsin-Hsuan Huang

Page 1 of 1

It is certified that error appears in the above-identified patent and that said Letters Patent is hereby corrected as shown below:

In the Claims

- (1) In Column 29, line 40, Claim 8 of the issued patent reads as " $0 < (R_{n1}-R_{n2})/(R_{n1}+R_{n2}) < 1.5$ ", but it should read as " $0 < (R_{n1}-R_{n2})/(R_{n1}+R_{n2}) < 1.5$ ".
- (2) In Column 30, line 28, Claim 21 of the issued patent reads as "a first lens element having an abject-side surface...", but it should read as "a first lens element having an object-side surface...".
- (3) In Column 30, line 39, Claim 21 of the issued patent reads as "a sixth lens element...and an side surface...", but it should read as "a sixth lens element...and an image-side surface...".

Signed and Sealed this
Second Day of August, 2016



Michelle K. Lee
Director of the United States Patent and Trademark Office